

Tin Melting Front

This model is licensed under the COMSOL Software License Agreement 6.1. All trademarks are the property of their respective owners. See www.comsol.com/trademarks. This example demonstrates how to model phase transition by a moving boundary interface according to the Stefan problem. It is adapted from the benchmark study in Ref. 1.

A square cavity containing both solid and liquid tin is submitted to a temperature difference between left and right boundaries. Fluid and solid parts are solved in separate domains sharing a moving melting front (see Figure 1). The position of this boundary through time is calculated according to the Stefan energy balance condition.



Figure 1: Square cavity with moving phase interface.

In the molten tin domain, motion generated by natural convection is expected due to the temperature gradient. This motion, in turn, influences the front displacement.

Model Definition

The geometry presented in Figure 2 shows a square of side length 10 cm filled with pure tin. The left and right boundaries are maintained at 508 K and 503 K, respectively.

Because the fusion temperature of pure tin is 505 K, both liquid and solid phases co-exist in the square.



Figure 2: Geometry and boundary conditions at initial time.

The initial temperature distribution is assumed to vary linearly in the horizontal direction as shown in Figure 3.



Figure 3: Initial temperature profile.

The melting front is the vertical line initially located at x = 6 cm where the temperature is 505 K.

The fluid motion in the liquid part on the left is modeled by the incompressible Navier-Stokes equations with Boussinesq approximation, as described in *Gravity* and *The Boussinesq Approximation* sections in the *CFD Module User's Guide*, with $T_{ref} = T_f$ the fusion temperature of tin. The reduced pressure formulation is used to enhance the accuracy of the buoyancy forces since they are relatively small compared to the other terms in the momentum balance.

As the metal melts, the solid-liquid interface moves toward the solid side. The energy balance at this front is expressed by the Stefan condition:

$$\rho_0 \Delta H \mathbf{v} \cdot \mathbf{n} = (\Phi_l - \Phi_s) \cdot \mathbf{n} \tag{1}$$

where ΔH is the latent heat of fusion, equal to 60 kJ/kg, **v** (SI unit: m/s) is the front velocity vector, **n** is the normal vector at the front, and Φ_l and Φ_s (SI unit: W/m²) are the heat fluxes coming from the liquid and solid sides, respectively (see Figure 4).



Figure 4: Heat fluxes at the melting front.

Table 1 reviews the material properties of tin (Ref. 2) used in this model.

PARAMETER	DESCRIPTION	VALUE
ρ ₀	Density	7500 kg/m ³
C_p	Heat capacity	200 J/(kg·K)
k	Thermal conductivity	60 W/(m·K)
α_p	Coefficient of thermal expansion	2.67·10 ⁻⁴ K ⁻¹
μ	Dynamic viscosity	6.0·10 ⁻³ Pa·s

TABLE I: MATERIAL PROPERTIES OF TIN.

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PARAMETER	DESCRIPTION	VALUE
T_{f}	Fusion temperature	505 K
ΔH	Latent heat of fusion	60 kJ/kg

Results and Discussion

Figure 5 shows the velocity profile in the fluid domain. The convective cell due to buoyancy increases the melting speed at the upper part of the cavity.



Figure 5: Velocity profile in the fluid at the end of the simulation.

At the end of the simulation, the melting front does not move anymore because balance between left and right adjacent fluxes has been reached. In Figure 6, the temperature profile is represented jointly by a surface plot for temperature distribution and a velocity arrow plot.



Figure 6: Temperature profile at the end of the simulation.

Notes About the COMSOL Implementation

The quantities Φ_l and Φ_s , illustrated in Figure 4, can be computed on each side of the melting front using the up and down operators. The components of $\Phi_l - \Phi_s$ are then given by up(ht.tfluxx)-down(ht.tfluxx) and up(ht.tfluxy)-down(ht.tfluxy). However, this method evaluates the temperature gradient which may lead to imprecisions due to the mesh discretization. Instead, the quantity $(\Phi_l - \Phi_s) \cdot \mathbf{n}$, involved in Equation 1, is more precisely evaluated through the Lagrange multiplier for temperature, T_lm. This variable is available when weak constraints are enabled in the region of interest, as it is the case here with the fixed temperature constraint at the melting front. For more information about weak constraints, refer to the *Weak Constraint* section in the *COMSOL Multiphysics Reference Manual*.

To handle the melting front movement, a mesh deformation is necessary. During such a transformation, matter from solid tin is removed while the same amount of liquid tin is added to the fluid. The appropriate tool for deforming the mesh without reflecting any

expansion or contraction effects to the material properties is the **Deformed Geometry** node under **Definitions**.

References

1. F. Wolff and R. Viskanta, "Solidification of a Pure Metal at a Vertical Wall in the Presence of Liquid Superheat," *Int.J. Heat and Mass Transfer*, vol. 31, no. 8, pp. 1735–1744, 1988.

2. V. Alexiades, N. Hannoun, and T.Z. Mai, "Tin Melting: Effect of Grid Size and Scheme on the Numerical Solution," *Proc. 5th Mississippi State Conf. Differential Equations and Computational Simulations*, pp. 55–69, 2003.

Application Library path: Heat_Transfer_Module/Phase_Change/ tin_melting_front

Modeling Instructions

From the File menu, choose New.

NEW

In the New window, click 🔗 Model Wizard.

MODEL WIZARD

- I In the Model Wizard window, click **2D**.
- 2 In the Select Physics tree, select Heat Transfer>Conjugate Heat Transfer>Laminar Flow.
- 3 Click Add.
- 4 Click 🔿 Study.
- 5 In the Select Study tree, select General Studies>Time Dependent.
- 6 Click **M** Done.

GLOBAL DEFINITIONS

Parameters I

- I In the Model Builder window, under Global Definitions click Parameters I.
- 2 In the Settings window for Parameters, locate the Parameters section.

Name	Expression	Value	Description
k_Sn	60[W/(m*K)]	60 W/(m·K)	Thermal conductivity
Cp_Sn	200[J/(kg*K)]	200 J/(kg·K)	Specific heat capacity
alpha_Sn	2.67e-4[1/K]	2.67E-4 I/K	Coefficient of thermal expansion
mu_Sn	6e-3[Pa*s]	0.006 Pa·s	Kinematic viscosity
rho_Sn	7500[kg/m^3]	7500 kg/m³	Density
DelH	60[kJ/kg]	60000 J/kg	Latent heat of fusion
Tf	505[K]	505 K	Melting point

508 K

503 K

Hot wall temperature Cold wall temperature

3 In the table, enter the following settings:

GEOMETRY I

Τh

Тс

Square 1 (sq1)

I In the **Geometry** toolbar, click Square.

508[K]

503[K]

- 2 In the Settings window for Square, locate the Size section.
- 3 In the Side length text field, type 0.1.
- 4 Click to expand the Layers section. In the table, enter the following settings:

Layer name	Thickness (m)		
Layer 1	0.06		

- 5 Select the Layers to the left check box.
- 6 Clear the Layers on bottom check box.
- 7 In the Geometry toolbar, click 📗 Build All.
- 8 Click the 🕂 Zoom Extents button in the Graphics toolbar.

MATERIALS

Tin (Solid)

- I In the Materials toolbar, click 🚦 Blank Material.
- 2 In the Settings window for Material, type Tin (Solid) in the Label text field.
- 3 Select Domain 2 only.

Before defining the material properties, set the solid and fluid domains in the physics interfaces to let COMSOL Multiphysics flag what properties you need to specify.

LAMINAR FLOW (SPF)

- I In the Model Builder window, under Component I (compl) click Laminar Flow (spf).
- **2** Select Domain 1 only.

HEAT TRANSFER IN SOLIDS AND FLUIDS (HT)

- I In the Model Builder window, under Component I (compl) click Heat Transfer in Solids and Fluids (ht).
- **2** In the **Settings** window for **Heat Transfer in Solids and Fluids**, locate the **Physical Model** section.
- **3** In the $T_{\rm ref}$ text field, type Tf.

Fluid I

- In the Model Builder window, under Component I (compl)>
 Heat Transfer in Solids and Fluids (ht) click Fluid I.
- **2** Select Domain 1 only.

MATERIALS

Tin (Solid) (mat1)

- I In the Model Builder window, under Component I (compl)>Materials click Tin (Solid) (matl).
- 2 In the Settings window for Material, locate the Material Contents section.
- **3** In the table, enter the following settings:

Property	Variable	Value	Unit	Property group
Thermal conductivity	k_iso ; kii = k_iso, kij = 0	k_Sn	W/(m·K)	Basic
Density	rho	rho_Sn	kg/m³	Basic
Heat capacity at constant pressure	Ср	Cp_Sn	J/(kg·K)	Basic

Duplicate this material: selecting the fluid domain will make COMSOL Multiphysics enquire for the missing needed parameters.

Tin (Solid) I (mat2)

Right-click Component I (compl)>Materials>Tin (Solid) (matl) and choose Duplicate.

Tin (Liquid)

- In the Model Builder window, expand the Component I (comp1)>Materials>
 Tin (Solid) (mat1) node, then click Component I (comp1)>Materials>Tin (Solid) I (mat2).
- 2 In the Settings window for Material, type Tin (Liquid) in the Label text field.
- **3** Select Domain 1 only.
- 4 Locate the Material Contents section. In the table, enter the following settings:

Property	Variable	Value	Unit	Property group
Dynamic viscosity	mu	mu_Sn	Pa·s	Basic

HEAT TRANSFER IN SOLIDS AND FLUIDS (HT)

Initial Values 1

Define the initial temperature as a function of Xg, the first coordinate on the undeformed geometry.

- I In the Model Builder window, under Component I (compl)> Heat Transfer in Solids and Fluids (ht) click Initial Values I.
- 2 In the Settings window for Initial Values, locate the Initial Values section.
- **3** In the *T* text field, type Th-Xg/0.1[m]*(Th-Tc).

LAMINAR FLOW (SPF)

- I In the Model Builder window, under Component I (compl) click Laminar Flow (spf).
- 2 In the Settings window for Laminar Flow, locate the Physical Model section.
- 3 From the Compressibility list, choose Incompressible flow.
- 4 Select the Include gravity check box.
- **5** Select the **Use reduced pressure** check box.

HEAT TRANSFER IN SOLIDS AND FLUIDS (HT)

In the Model Builder window, under Component I (compl) click Heat Transfer in Solids and Fluids (ht).

Temperature I

- I In the Physics toolbar, click Boundaries and choose Temperature.
- 2 Select Boundary 1 only.

- 3 In the Settings window for Temperature, locate the Temperature section.
- **4** In the T_0 text field, type Th.

Temperature 2

- I In the Physics toolbar, click Boundaries and choose Temperature.
- 2 Select Boundary 7 only.
- 3 In the Settings window for Temperature, locate the Temperature section.
- **4** In the T_0 text field, type Tc.

Phase Change Interface 1

- I In the Physics toolbar, click Boundaries and choose Phase Change Interface.
- 2 Select Boundary 4 only.
- **3** In the **Settings** window for **Phase Change Interface**, locate the **Phase Change Interface** section.
- **4** In the $T_{\rm pc}$ text field, type Tf.
- **5** In the $L_{s \to f}$ text field, type DelH.
- 6 From the Solid side list, choose Downside.

LAMINAR FLOW (SPF)

In the Model Builder window, under Component I (compl) click Laminar Flow (spf).

Pressure Point Constraint I

- I In the Physics toolbar, click 💭 Points and choose Pressure Point Constraint.
- 2 Select Point 1 only.

The model only contains information about the pressure gradient and estimates the pressure field up to a constant. To define this constant, you arbitrarily fix the pressure at a point.

MULTIPHYSICS

Nonisothermal Flow 1 (nitf1)

- I In the Model Builder window, under Component I (compl)>Multiphysics click Nonisothermal Flow I (nitfl).
- 2 In the Settings window for Nonisothermal Flow, locate the Material Properties section.
- **3** Select the **Boussinesq approximation** check box.
- 4 From the Specify density list, choose Custom, linearized density.
- **5** From the ρ_{ref} list, choose **From material**.

6 In the $\alpha_{p,0}$ text field, type alpha_Sn.

COMPONENT I (COMPI)

Deforming Domain I

- I In the Definitions toolbar, click ••• Deformed Geometry and choose Domains> Deforming Domain.
- 2 In the Settings window for Deforming Domain, locate the Domain Selection section.
- 3 From the Selection list, choose All domains.
- 4 Locate the Smoothing section. From the Mesh smoothing type list, choose Laplace.

Prescribed Normal Mesh Displacement I

- I In the Definitions toolbar, click • • Deformed Geometry and choose Boundaries> Prescribed Normal Mesh Displacement.
- **2** Select Boundaries 1–3 and 5–7 only.

MESH I

- I In the Model Builder window, under Component I (compl) click Mesh I.
- 2 In the Settings window for Mesh, locate the Physics-Controlled Mesh section.
- 3 From the Element size list, choose Fine.
- 4 Click 📗 Build All.

STUDY I

Step 1: Time Dependent

- I In the Model Builder window, under Study I click Step I: Time Dependent.
- 2 In the Settings window for Time Dependent, locate the Study Settings section.
- 3 Click Range.
- 4 In the Range dialog box, type 100 in the Step text field.
- 5 In the **Stop** text field, type 10000.
- 6 Click Replace.

For more robust convergence, tighten the relative tolerance, which controls the size of the time steps taken by the solver.

- 7 In the Settings window for Time Dependent, locate the Study Settings section.
- 8 From the Tolerance list, choose User controlled.
- 9 In the Relative tolerance text field, type 1e-4.

Solution 1 (soll)

- I In the Study toolbar, click The Show Default Solver.
- 2 In the Model Builder window, expand the Solution I (soll) node.
- In the Model Builder window, expand the Study I>Solver Configurations>
 Solution I (soll)>Dependent Variables I node, then click
 Material mesh displacement (compl.material.disp).
- 4 In the Settings window for Field, locate the Scaling section.
- 5 From the Method list, choose From parent.
- 6 In the Study toolbar, click **=** Compute.

RESULTS

Temperature (ht)

This default plot shows the temperature profile. To reproduce Figure 6, add arrows of the velocity field to see the relation between temperature and velocity.

Arrow Surface 1

- I In the **Temperature (ht)** toolbar, click \rightarrow **Arrow Surface**.
- 2 In the Settings window for Arrow Surface, click Replace Expression in the upper-right corner of the Expression section. From the menu, choose Component I (compl)> Laminar Flow>Velocity and pressure>u,v Velocity field (spatial and material frames).
- 3 Locate the Coloring and Style section. From the Arrow type list, choose Cone.
- 4 From the Color list, choose Black.
- 5 In the Temperature (ht) toolbar, click 💿 Plot.

Velocity (spf)

This default plot shows the velocity profile in the fluid region. To reproduce Figure 5, add arrows of the velocity field to visualize the convective flow direction.

I In the Model Builder window, under Results click Velocity (spf).

Arrow Surface 1

- I In the Velocity (spf) toolbar, click \rightarrow Arrow Surface.
- 2 In the Settings window for Arrow Surface, click Replace Expression in the upper-right corner of the Expression section. From the menu, choose Component I (compl)> Laminar Flow>Velocity and pressure>u,v Velocity field (spatial and material frames).
- 3 Locate the Coloring and Style section. From the Arrow type list, choose Cone.
- 4 From the Color list, choose Black.

5 In the Velocity (spf) toolbar, click **I** Plot.

Finally, plot the mesh deformation as follows.

Mesh Deformation

- I In the Home toolbar, click 🚛 Add Plot Group and choose 2D Plot Group.
- 2 In the Settings window for 2D Plot Group, type Mesh Deformation in the Label text field.

Mesh I

- I In the Mesh Deformation toolbar, click 🗡 Mesh.
- 2 In the Settings window for Mesh, locate the Coloring and Style section.
- **3** From the **Element color** list, choose **None**.
- 4 From the Wireframe color list, choose Blue.

Selection I

- I Right-click Mesh I and choose Selection.
- **2** Select Domain 1 only.
- **3** In the Mesh Deformation toolbar, click **I** Plot.

Mesh 2

- I In the Model Builder window, under Results>Mesh Deformation right-click Mesh I and choose Duplicate.
- 2 In the Settings window for Mesh, click to expand the Title section.
- 3 From the Title type list, choose None.
- 4 Locate the Coloring and Style section. From the Wireframe color list, choose Red.

Selection I

- I In the Model Builder window, expand the Mesh 2 node, then click Selection I.
- 2 In the Settings window for Selection, locate the Selection section.
- **3** Click to select the **EXACTIVATE Selection** toggle button.
- **4** Select Domain 2 only.

5 In the **Mesh Deformation** toolbar, click **O Plot**.

The plot should look like that in the figure below.



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