

Double-Pipe Heat Exchanger

A double-pipe heat exchanger consists of two concentric pipes often performing a U-turn. Due to low costs, it has a large range of applications especially in the chemical process industry. Another advantage is that it can operate at very high pressures. For different scopes, the double-pipe heat exchanger can be stacked in series.

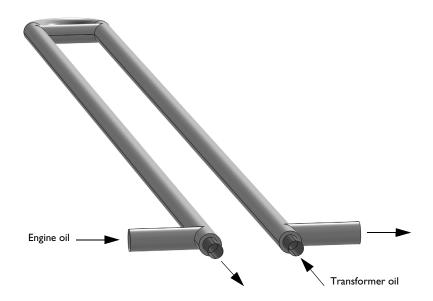


Figure 1: Geometry and concept of the double-pipe heat exchanger.

This tutorial shows how to efficiently model a double-pipe heat exchanger and focuses on preparing the geometry in order to build a suitable mesh manually. In addition, typical postprocessing options are shown.

Model Definition

The concept and basic geometry of the double-pipe heat exchanger is shown in Figure 1. The heat exchanger is made of high tensile steel (Steel AISI 4340). The radii of the concentric pipes are 2.55 cm and 4.8 cm, while the overall length is about 6 m. Due to this high aspect ratio, the mesh has to be carefully handled.

Engine oil at 130°C flows through the outer pipe and is cooled by a transformer oil at 60°C, flowing in countercurrent through the inner pipe to prevent the engine oil from overheating. The material properties of both oils depend on the temperature, and thus the Nonisothermal Flow predefined multiphysics coupling is used.

FLOW REGIME

To decide whether the flow is laminar or turbulent, estimate the Reynolds number beforehand. The Reynolds number for flows inside a pipe is defined as

$$Re = \frac{\rho v D_H}{\mu}$$

where ρ is the density of the fluid, v the typical velocity (taken as the inlet velocity), μ the viscosity, and D_H the hydraulic diameter. For the inner pipe, D_H is equal to the diameter of the pipe, and for the outer pipe it is the difference between the pipes radii. Adhere to the typical values in Table 1 to evaluate Re.

TABLE I: TYPICAL OUANTITIES FOR THE REYNOLDS NUMBER.

Quantity	Symbol	Inner pipe	Outer pipe
Density	ρ	850 kg/m ³	825 kg/m ³
Inlet velocity	v	0.205 m/s	0.09 m/s
Typical length	D_H	5.1 cm	1.3 cm
Dynamic viscosity	μ	5·10 ⁻³ Pa·s	I·I0 ⁻³ Pa·s

The Reynolds numbers for the inner and outer pipes are about 1800 and 1000, respectively. Based on this approximation the Nonisothermal Flow multiphysics coupling in laminar regime is used.

Meanwhile, the densities of the two separated fluids can be considered constant thanks to small temperature variations in each of the inner and outer pipes. Both fluid flows can then be modeled by incompressible formulations.

BOUNDARY CONDITIONS

The body of the heat exchanger is modeled as a shell in 3D. This requires special boundary conditions for the flow and heat transport equations. The interior wall condition separates the pipes and applies a no slip condition for the flow on both sides.

To account for the in-plane heat flux in the shell, the **Thin Layer** boundary condition is applied. This boundary condition simulates heat transfer in thin shell structures. Here, the shell is made of steel with a 7 mm thickness.

The inlet boundary condition applies a laminar inflow profile at the pipe's ends. Refer to the Heat Transfer Module User's Guide for more information about the settings for this boundary condition. The engine oil enters the outer pipe at 130°C and with an average velocity of 0.09 m/s. The transformer oil enters the inner pipe at 60°C and with an average velocity of 0.205 m/s.

The outlets are connected to pipes of same diameter. For this configuration, the Suppress backflow option in the Outlet feature is particularly suited.

At exterior boundaries, the model assumes thermal insulation because the losses to the outside are considered negligible.

Results and Discussion

Figure 2 shows the temperature distribution along the center plane. The transformer oil is heated up by 9°C to 69°C while the engine oil is cooled by 7°C to 123°C.

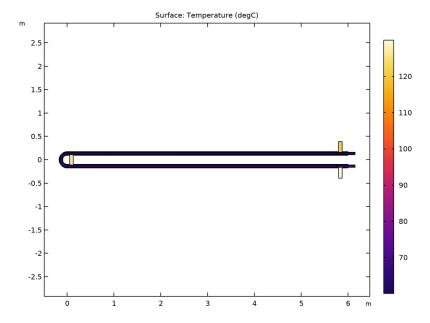


Figure 2: Temperature field in the central plane, zoomed at inlet and outlet regions.

The next plot shows the velocity field.



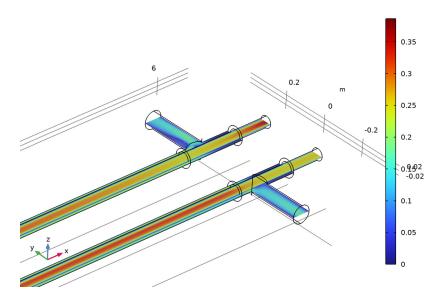


Figure 3: Velocity magnitude inside the pipes, zoomed at inlet and outlet regions.

The calculated pressure drops are close to 155 Pa for the inner pipe and close to 1350 Pa for the outer pipe.

The equivalent heat transfer coefficient describes the heat exchanger's performance. It is given by

$$h_{\rm eq} = \frac{P}{A(T_{\rm hot} - T_{\rm cold})} \tag{1}$$

where P is the total exchanged power and A is the surface area of the interface between the two fluids. In this model the value of h_{eq} is about 42 W/(m²·K).

Notes About the COMSOL Implementation

Setting up of the Nonisothermal Flow multiphysics coupling is straightforward according to the descriptions above. Due to the high nonlinearity in the model, initial values affect convergence. It is sufficient to set the initial temperature to $(T_{\text{hot}} + T_{\text{cold}})/2$.

Furthermore, the fluids that are considered incompressible would have densities equal to

a reference value, $\rho(T_{ref})$, taken at a reference temperature of T_{cold} at inner pipes and T_{hot} at outer pipes.

In this tutorial, using a physics-induced mesh leads to a large number of mesh elements. The long straight parts of the pipes can be meshed more efficiently with a swept mesh without losing accuracy. Therefore, the geometry needs to be divided into three parts: the U-turn, the straight parts, and the inlets/outlets (see Figure 4). The Modeling Instructions section below contains the steps for preparing and meshing the geometry as well as the postprocessing part.



Figure 4: Geometry of the double-pipe heat exchanger divided into three parts.

Application Library path: Heat Transfer Module/Heat Exchangers/ double pipe heat exchanger

Reference

1. H. S. Lee, Thermal Design, John Wiley & Sons, 2010.

Modeling Instructions

APPLICATION LIBRARIES

- I From the File menu, choose Application Libraries.
- 2 In the Application Libraries window, select Heat Transfer Module>Heat Exchangers> double_pipe_heat_exchanger_preset in the tree.
- 3 Click Open.

COMPONENT I (COMPI)

To evaluate the equivalent heat transfer coefficient after the simulation, define a nonlocal integration coupling over the interior walls.

DEFINITIONS (COMPI)

Average Over Interior Wall

- I In the Definitions toolbar, click // Nonlocal Couplings and choose Average.
- 2 In the Settings window for Average, type Average Over Interior Wall in the Label text field.
- 3 Locate the Source Selection section. From the Geometric entity level list, choose Boundary.
- 4 From the Selection list, choose Interior Walls.

The physics-controlled mesh is satisfying for fluid flow models with boundary layers at all no-slip boundaries. The gradient along the pipes is expected to be very low compared to the gradient perpendicular to the pipes cross-sections. Hence, a swept mesh is an appropriate choice for meshing the straight part of the pipes, reducing the computational costs while keeping accuracy. Before it is applicable, the geometry needs to be prepared to have the straight part of the pipes as separate domains. This can be done by partitioning the geometry with work planes. The predefined selections in **Component I>Definitions** ensure that the physical settings still apply to the correct entities, even after the partitioning operations.

GEOMETRY I

Work Plane I (wbl)

- I In the Geometry toolbar, click Swork Plane.
- 2 In the Settings window for Work Plane, locate the Plane Definition section.
- 3 From the Plane type list, choose Face parallel.
- 4 On the object imp1, select Boundary 27 only.

It might be easier to select the correct boundary by using the Selection List window. To open this window, in the Home toolbar click Windows and choose Selection List. (If you are running the cross-platform desktop, you find **Windows** in the main menu.)

- 5 In the Offset in normal direction text field, type 0.4.
- 6 Select the Reverse normal direction check box.

Partition Objects I (par I)

I In the Geometry toolbar, click Booleans and Partitions and choose Partition Objects.

- **2** Select the object **imp1** only.
- 3 In the Settings window for Partition Objects, locate the Partition Objects section.
- 4 From the Partition with list, choose Work plane.

Work Plane 2 (wb2)

- I In the Geometry toolbar, click Work Plane.
- 2 In the Settings window for Work Plane, locate the Plane Definition section.
- 3 From the Plane type list, choose Face parallel.
- 4 On the object parl, select Boundary 40 only.
- 5 In the Offset in normal direction text field, type 6.
- 6 Select the Reverse normal direction check box.

Partition Objects 2 (par2)

- I In the Geometry toolbar, click Booleans and Partitions and choose Partition Objects.
- 2 Select the object parl only.
- 3 In the Settings window for Partition Objects, locate the Partition Objects section.
- 4 From the Partition with list, choose Work plane.
- 5 Click **Build All Objects**.

The mesh can be set up. Start by the inlet and outlet parts, then sweep the mesh through the straight pipes. The U-turn again is meshed with free tetrahedral elements. The last step is to introduce the boundary-layer mesh at all no-slip walls.

MESH I

Free Tetrahedral I

In the Mesh toolbar, click A Free Tetrahedral.

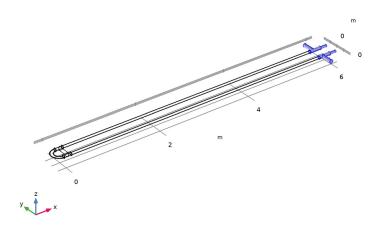
Size

- I In the Model Builder window, click Size.
- 2 In the Settings window for Size, locate the Element Size section.
- 3 From the Calibrate for list, choose Fluid dynamics.
- 4 From the Predefined list, choose Finer.

Free Tetrahedral I

- I In the Model Builder window, click Free Tetrahedral I.
- 2 In the Settings window for Free Tetrahedral, locate the Domain Selection section.
- 3 From the Geometric entity level list, choose Domain.

4 Select Domains 7–10 only.



Size 1

- I In the Mesh toolbar, click Size Attribute and choose Extra Fine.
- 2 In the Settings window for Size, locate the Geometric Entity Selection section.
- 3 From the Geometric entity level list, choose Boundary.
- 4 Select Boundaries 27, 30, 33, and 36 only.
- 5 Locate the Element Size section. From the Calibrate for list, choose Fluid dynamics.
- 6 Click the Custom button.
- 7 Locate the Element Size Parameters section. Select the Maximum element size check box.
- 8 In the associated text field, type 0.009.
- 9 Click Pauld Selected.

Swebt I

- I In the Mesh toolbar, click A Swept.
- 2 In the Settings window for Swept, locate the Domain Selection section.
- 3 From the Geometric entity level list, choose Domain.
- **4** Select Domains 3–6 only.

Distribution I

I Right-click Swept I and choose Distribution.

- 2 In the Settings window for Distribution, locate the Distribution section.
- 3 From the Distribution type list, choose Predefined.
- 4 In the Number of elements text field, type 150.
- 5 In the Element ratio text field, type 5.
- 6 Select the Symmetric distribution check box.
- 7 Click **Build Selected**.

Free Tetrahedral 2

- I In the Mesh toolbar, click A Free Tetrahedral.
- 2 In the Settings window for Free Tetrahedral, click Pauld Selected.

Boundary Layers 1

In the Mesh toolbar, click Boundary Layers.

In this geometry it is possible to generate the boundary layer elements without the corner splitting. This will result in a more homogeneous boundary layer mesh.

- I In the Settings window for Boundary Layers, click to expand the Corner Settings section.
- 2 From the Handling of sharp edges list, choose No special handling.
- 3 Click to expand the Transition section. Clear the Smooth transition to interior mesh check box.

Boundary Layer Properties

- I In the Model Builder window, expand the Boundary Layers I node, then click **Boundary Layer Properties.**
- 2 In the Settings window for Boundary Layer Properties, locate the Geometric Entity Selection section.
- 3 From the Selection list, choose Steel Walls.
- 4 Locate the Layers section. In the Number of layers text field, type 2.
- 5 In the Thickness adjustment factor text field, type 5.
- 6 Click III Build All.

STUDY I

Switch the default nonlinear solver to get faster convergence.

Solution I (soll)

- I In the Study toolbar, click how Default Solver.
- 2 In the Model Builder window, expand the Solution I (soll) node.

- 3 In the Model Builder window, expand the Study I>Solver Configurations> Solution I (soll)>Stationary Solver I node, then click Segregated I.
- 4 In the Settings window for Segregated, locate the General section.
- 5 From the Stabilization and acceleration list, choose Anderson acceleration.
- 6 In the Model Builder window, expand the Study I>Solver Configurations> Solution I (soll)>Stationary Solver I>AMG, fluid flow variables (spf) node, then click Multigrid I.
- 7 In the Settings window for Multigrid, locate the General section.
- 8 Select the Compact aggregation check box.
- 9 In the Study toolbar, click **Compute**.

RESULTS

Velocity (sbf)

To create the plot shown in Figure 3 change the settings of the default velocity plot.

Slice

- I In the Model Builder window, expand the Velocity (spf) node, then click Slice.
- 2 In the Settings window for Slice, locate the Plane Data section.
- 3 From the Plane list, choose xy-planes.
- 4 In the Planes text field, type 1.
- 5 In the Model Builder window, click Slice.
- 6 In the Velocity (spf) toolbar, click **Plot**.
- 7 Use the **Graphics** toolbox to get a satisfying view.

Cut Plane I

I In the Results toolbar, click Cut Plane.

A 2D plot provides a better view of the temperature distribution along the pipes. Therefore, a new dataset is created and then used for a 2D surface plot. Figure 2 shows the temperature distribution in the center plane of the heat exchanger.

- 2 In the Settings window for Cut Plane, locate the Plane Data section.
- 3 From the Plane list, choose xy-planes.

Temperature (2D Center Plane)

- I In the Results toolbar, click 2D Plot Group.
- 2 In the Settings window for 2D Plot Group, type Temperature (2D Center Plane) in the Label text field.

3 Locate the Data section. From the Dataset list, choose Cut Plane 1.

Surface 1

- I In the Temperature (2D Center Plane) toolbar, click Surface.
- 2 In the Settings window for Surface, click Replace Expression in the upper-right corner of the Expression section. From the menu, choose Component I (compl)> Heat Transfer in Fluids>Temperature>T - Temperature - K.
- 3 Locate the Expression section. From the Unit list, choose degC.
- 4 Locate the Coloring and Style section. From the Color table list, choose ThermalDark.
- 5 In the Model Builder window, click Surface 1.
- 6 From the Color table list, choose HeatCamera.
- **7** Use the **Graphics** toolbox to get a satisfying view.

The equivalent heat transfer coefficient can be calculated according to Equation 1.

Heat Transfer Coefficient

- I In the Results toolbar, click (8.5) Global Evaluation.
- 2 In the Settings window for Global Evaluation, type Heat Transfer Coefficient in the Label text field.
- **3** Locate the **Expressions** section. In the table, enter the following settings:

Expression	Unit	Description
aveop1(-ht.ntflux)/(T_hot-T_cold)	W/(m^2*K)	

4 Click **= Evaluate**.

TABLE

I Go to the **Table** window.

You should get around 42 W/($m^2 \cdot K$).

Evaluate the outlet temperatures and the pressure drops in the pipes.

RESULTS

Outlet Temperature, Transformer Oil

- I In the Results toolbar, click 8.85 More Derived Values and choose Average> Surface Average.
- 2 In the Settings window for Surface Average, type Outlet Temperature, Transformer Oil in the Label text field.

- 3 Locate the Selection section. From the Selection list, choose Inner Pipe, Outlet.
- 4 Click Replace Expression in the upper-right corner of the Expressions section. From the menu, choose Component I (compl)>Heat Transfer in Fluids>Temperature>T -Temperature - K.
- **5** Locate the **Expressions** section. In the table, enter the following settings:

Expression	Unit	Description
T	degC	Temperature

6 Click **= Evaluate**.

TABLE

Go to the **Table** window.

Outlet Temperature, Engine Oil

- I Right-click Outlet Temperature, Transformer Oil and choose Duplicate.
- 2 In the Settings window for Surface Average, type Outlet Temperature, Engine Oil in the Label text field.
- 3 Locate the Selection section. From the Selection list, choose Outer Pipe, Outlet.
- 4 Click **= Evaluate**.
- **5** Go to the **Table** window.

The transformer oil is heated up to 69°C while the engine oil is cooled to 123°C.

Inlet Pressure, Transformer Oil

I In the Results toolbar, click 8.85 More Derived Values and choose Average> Surface Average.

The pressure drop is the difference between the inlet and outlet pressure. Because the pressure at the outlets is approximately zero, it is sufficient to calculate the inlet pressures.

- 2 In the Settings window for Surface Average, type Inlet Pressure, Transformer Oil in the Label text field.
- 3 Locate the Selection section. From the Selection list, choose Inner Pipe, Inlet.
- 4 Click Replace Expression in the upper-right corner of the Expressions section. From the menu, choose Component I (compl)>Laminar Flow>Velocity and pressure>p - Pressure -Pa.
- 5 Click ▼ next to **= Evaluate**, then choose **New Table**.
- 6 Go to the Table window.

Inlet Pressure, Engine Oil

- I Right-click Inlet Pressure, Transformer Oil and choose Duplicate.
- 2 In the Settings window for Surface Average, type Inlet Pressure, Engine Oil in the Label text field.
- 3 Locate the Selection section. From the Selection list, choose Outer Pipe, Inlet.
- 4 Click **= Evaluate**.
- **5** Go to the **Table** window.

The pressure drop at the inner and outer pipes are close to 155 Pa and 1350 Pa, respectively.