

Continuous Casting — Apparent Heat Capacity Method

This example simulates the process of continuous casting of a metal rod from a molten state (Figure 1). To optimize the casting process in terms of casting rate and cooling, it is helpful to model the thermal and fluid dynamics aspects of the process. To get accurate results, you must model the melt flow field in combination with the heat transfer and phase change. The model includes the phase transition from melt to solid, both in terms of latent heat and the varying physical properties. Continuous Casting — Arbitrary Lagrangian-Eulerian Method is a variant of this model using the Phase Change Interface boundary condition.

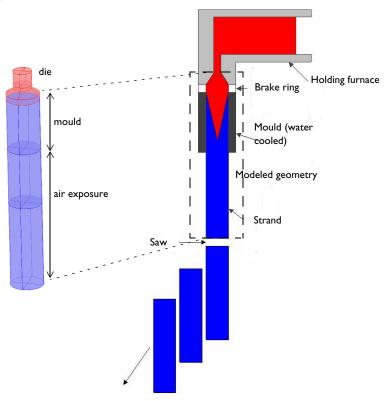


Figure 1: Continuous metal-casting process with a view of the modeled section.

This example simplifies the rod's 3D geometry in Figure 1 to an axisymmetric 2D model in the *rz*-plane. Figure 2 shows the dimensions of the 2D geometry.

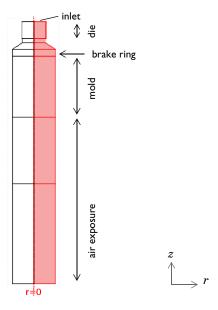


Figure 2: 2D axisymmetric model of the casting process.

As the melt cools down in the mold it solidifies. The phase transition releases latent heat, which the model includes. Furthermore, for metal alloys, the transition is often spread out over a temperature range. As the material solidifies, the material properties change considerably. Finally, the model also includes the "mushy" zone — a mixture of solid and melted material that occurs due to the rather broad transition temperature of the alloy and the solidification kinetics.

This example models the casting process as being stationary using the Heat Transfer in Fluids interface combined with the Laminar Flow interface.

Model Definition

The process operates at steady state, because it is a continuous process. The heat transport is described by the equation:

$$\rho C_p \mathbf{u} \cdot \nabla T + \nabla \cdot (-k \nabla T) \, = \, Q$$

where k, C_p , and Q denote thermal conductivity, specific heat, and heating power per unit volume (heat source term), respectively.

As the melt cools down in the mold, it solidifies. During the phase transition, a significant amount of latent heat is released. The total amount of heat released per unit mass of alloy during the transition is given by the change in enthalpy, ΔH . In addition, the specific heat capacity, C_p , also changes considerably during the transition.

As opposed to pure metals, an alloy generally undergoes a broad temperature transition zone, over several kelvin, in which a mixture of both solid and molten material co-exist in a "mushy" zone. To account for the latent heat related to the phase transition, the Apparent Heat capacity method is used through the Heat Transfer with Phase Change domain condition. The half-width of the transition interval, ΔT , is set to 10 K in this case, and represents half the transition temperature span.

This example models the laminar flow by describing the fluid velocity, **u**, and the pressure, p, according to the equations

$$\begin{split} \rho \frac{\partial \mathbf{u}}{\partial t} + \rho \mathbf{u} \cdot \nabla \mathbf{u} &= \nabla \cdot \left[-p \mathbf{I} + \mu (\nabla \mathbf{u} + (\nabla \mathbf{u})^T) - \left(\frac{2\mu}{3} - \kappa \right) (\nabla \cdot \mathbf{u}) \mathbf{I} \right] + \mathbf{F} \\ \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) &= 0 \end{split}$$

where ρ is the density (in this case constant), μ is the viscosity, and κ is the dilatational viscosity (here assumed to be zero). Here, the role of the source term, **F**, is to dampen the velocity at the phase-change interface so that it becomes that of the solidified phase after the transition. The source term follows from the equation (see Ref. 1)

$$\mathbf{F} = \frac{(1-\alpha)^2}{\alpha^3 + \varepsilon} A_{\text{mush}} (\mathbf{u} - \mathbf{u}_{\text{cast}})$$

where α can be seen as the volume fraction of the liquid phase; A_{mush} and ϵ represent arbitrary constants (A_{mush} should be large and ϵ small to produce a proper damping); and \mathbf{u}_{cast} is the velocity of the cast rod.

Table 1 reviews the material properties in this model.

TABLE I: MATERIAL PROPERTIES.

PROPERTY	SYMBOL	MELT	SOLID
Density	ρ (kg/m ³)	8500	8500
Heat capacity at constant pressure	$C_p \; (J/(kg \cdot K))$	530	380

TABLE I: MATERIAL PROPERTIES.

PROPERTY	SYMBOL	MELT	SOLID
Thermal conductivity	k (W/(m·K))	200	200
Dynamic viscosity	μ (N·s/m ²)	0.0434	-

Furthermore, the melting temperature, T_{m} , and enthalpy of phase change, ΔH , are set to 1356 K and 205 kJ/kg, respectively.

The model uses the parametric solver in combination with adaptive meshing to solve the problem efficiently. In particular, using an adaptive mesh makes it possible to resolve the steep gradients in the mushy zone at a comparatively low computational cost.

Results and Discussion

The plots in Figure 3 display the temperature and phase distributions, showing that the melt cools down and solidifies in the mold region. Interestingly, the transition zone stretches out toward the center of the rod because of poorer cooling in that area.

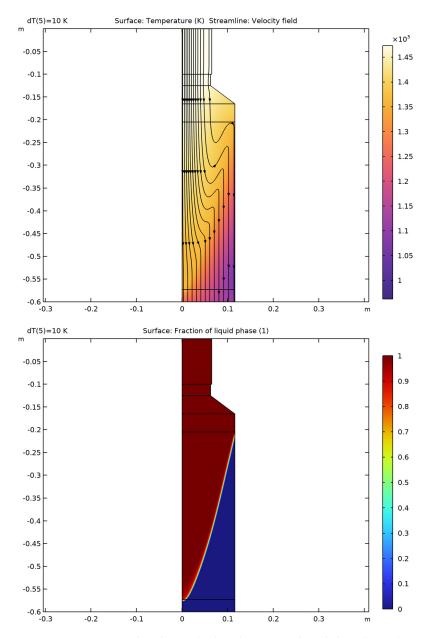


Figure 3: Temperature distribution (top) and fraction of liquid phase (bottom) near the inlet part of the cast at a casting rate of $1.6\ mm/s$.

With the modeled casting rate, the rod is fully solidified before leaving the mold (the first section after the die). This means that the process engineers can increase the casting rate without running into problems, thus increasing the production rate.

The phase transition occurs in a very narrow zone although the model uses a transition half width, ΔT , of 10 K. In reality it would be even more distinct if a pure metal were being cast but somewhat broader if the cast material were an alloy with a wider ΔT .

It is interesting to study in detail the flow field in the melt as it exits the die.

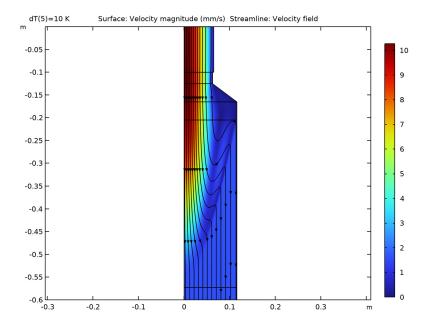


Figure 4: Velocity field with streamlines near the inlet part of the process.

In Figure 4, notice the disturbance in the streamlines close to the die wall resulting in a vortex. This eddy flow could create problems with nonuniform surface quality in a real process. Process engineers can thus use the model to avoid these problems and find an optimal die shape.

To help determine how to optimize process cooling, Figure 5 plots the conductive heat flux. It shows that the conductive heat flux is very large in the mold zone. This is a consequence of the heat released during the phase transition, which is cooled by the water-cooling jacket of the mold. An interesting phenomenon of the process is the peak of conductive heat flux appearing in the center of the flow at the transition zone.

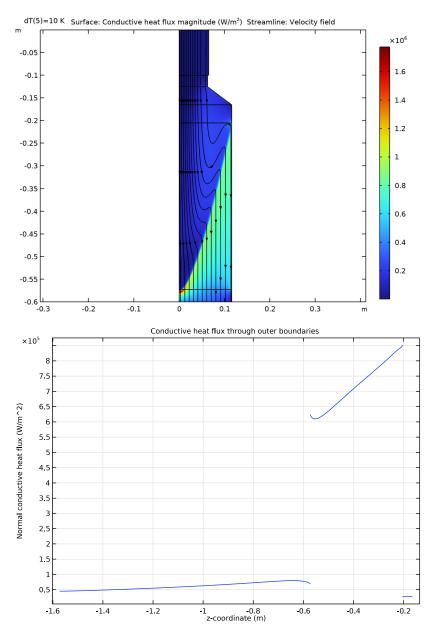


Figure 5: The cooling viewed as conductive heat flux in the domains (top), and through the outer boundary (the cooling zones) after the die (bottom).

Furthermore, by plotting the conductive heat flux at the outer boundary for the process as in the lower plot in Figure 5, you can see that a majority of the process cooling occurs in the mold. More interestingly, the heat flux varies along the mold wall length. This information can help in optimizing the cooling of the mold (that is, the cooling rate and choice of cooling method).

You solve the model using a built-in adaptive meshing technique. This is necessary because the transition zone — that is, the region where the phase change occurs — requires a fine discretization. Figure 6 depicts the final mesh of the model. Notice that the majority of the elements are concentrated to the transition zone.

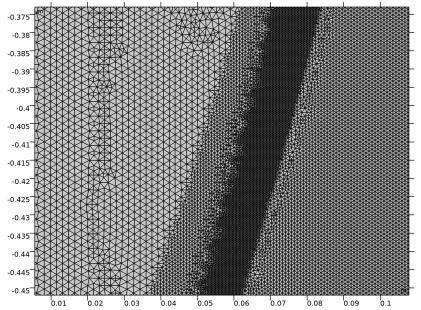


Figure 6: Close-up of the final computational mesh, resulting from the built-in adaptive technique.

The adaptive meshing technique allows for fast and accurate calculations even if the transition width is brought down to a low value, such as for pure metals.

Reference

1. V.R. Voller and C. Prakash, "A fixed grid numerical modeling methodology for convection — diffusion mushy region phase-change problems," *Int.J.Heat Mass Transfer*, vol. 30, pp. 1709–1719, 1987.

Application Library path: Heat Transfer Module/Thermal Processing/ continuous_casting_apparent_heat_capacity

Modeling Instructions

From the File menu, choose New.

NEW

In the New window, click Model Wizard.

MODEL WIZARD

- I In the Model Wizard window, click 2D Axisymmetric.
- 2 In the Select Physics tree, select Fluid Flow>Nonisothermal Flow>Laminar Flow.
- 3 Click Add.
- 4 Click Study.
- 5 In the Select Study tree, select General Studies>Stationary.
- 6 Click **Done**.

GLOBAL DEFINITIONS

Parameters 1

- I In the Model Builder window, under Global Definitions click Parameters I.
- 2 In the Settings window for Parameters, locate the Parameters section.
- 3 Click Load from File.
- 4 Browse to the model's Application Libraries folder and double-click the file continuous_casting_apparent_heat_capacity_parameters.txt.

Note, in particular, the value of the parameter dT, which represents the parameter ΔT in the Model Definition section. It will apply when you solve with adaptive mesh refinement because that solution stage is not related to a parametric study. It is then crucial that the value of dT matches that of the final parameter step for the parametric solution that is used as the initial solution.

DEFINITIONS

Variables 1

- I In the Home toolbar, click a= Variables and choose Local Variables.
- 2 In the Settings window for Variables, locate the Geometric Entity Selection section.
- 3 From the Geometric entity level list, choose Domain.
- **4** From the **Selection** list, choose **All domains**.

 Define the variables by loading the corresponding text file provided.
- 5 Locate the Variables section. Click **Load from File**.
- **6** Browse to the model's Application Libraries folder and double-click the file continuous_casting_apparent_heat_capacity_variables.txt.

GEOMETRY I

Rectangle I (rI)

- I In the Geometry toolbar, click Rectangle.
- 2 In the Settings window for Rectangle, locate the Size and Shape section.
- 3 In the Width text field, type 0.065.
- 4 In the **Height** text field, type 0.1.
- **5** Locate the **Position** section. In the **z** text field, type -0.1.
- 6 In the Geometry toolbar, click **Build All**.

Rectangle 2 (r2)

- I In the Geometry toolbar, click Rectangle.
- 2 In the Settings window for Rectangle, locate the Size and Shape section.
- 3 In the Width text field, type 0.0625.
- 4 In the Height text field, type 0.025.
- **5** Locate the **Position** section. In the **z** text field, type -0.125.
- 6 In the Geometry toolbar, click **Build All**.

Rectangle 3 (r3)

- I In the Geometry toolbar, click Rectangle.
- 2 In the Settings window for Rectangle, locate the Size and Shape section.
- 3 In the Width text field, type 0.11575.
- 4 In the **Height** text field, type 1.4075.
- **5** Locate the **Position** section. In the **z** text field, type -1.5725.

6 Click to expand the **Layers** section. In the table, enter the following settings:

Layer name	Thickness (m)
Layer 1	0.6
Layer 2	0.4
Layer 3	0.3675

7 In the Geometry toolbar, click **Build All**.

8 Click the Zoom Extents button in the Graphics toolbar.

Polygon I (poll)

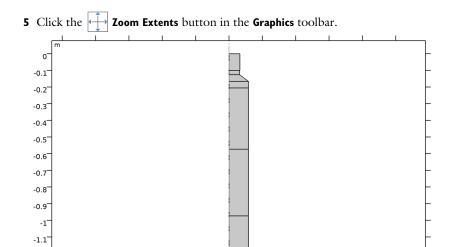
I In the Geometry toolbar, click / Polygon.

2 In the Settings window for Polygon, locate the Coordinates section.

3 In the table, enter the following settings:

r (m)	z (m)
0	-0.125
0	-0.165
0.11575	-0.165
0.0625	-0.125
0	-0.125

4 In the Geometry toolbar, click **Build All**.



This completes the geometry modeling stage.

-0.4

-0.2

l -0.6

-0.8

MATERIALS

-1.2 -1.3 -1.4 -1.5 -1.6

Now, add the following two materials to the model, labeled Solid Metal Alloy and Liquid Metal Alloy. The solid metal alloy is used in the Heat Transfer with Phase Change feature for the solid phase, while the liquid metal alloy is used for the liquid phase. The liquid metal alloy also defines fluid properties used in the Laminar Flow interface.

0.4

0.6

0.8

Solid Metal Alloy

- I In the Materials toolbar, click Blank Material.
- 2 In the Settings window for Material, type Solid Metal Alloy in the Label text field.
- **3** Locate the **Material Contents** section. In the table, enter the following settings:

Property	Variable	Value	Unit	Property group
Dynamic viscosity	mu	0.0434	Pa·s	Basic
Thermal conductivity	k_iso ; kii = k_iso, kij = 0	200	W/(m·K)	Basic

Property	Variable	Value	Unit	Property group
Density	rho	8500	kg/m³	Basic
Heat capacity at constant pressure	Ср	Cp_s	J/(kg·K)	Basic

Liquid Metal Alloy

- I In the Materials toolbar, click **Blank Material**.
- 2 In the Settings window for Material, type Liquid Metal Alloy in the Label text field.
- 3 Locate the Geometric Entity Selection section. From the Selection list, choose All domains.
- **4** Locate the **Material Contents** section. In the table, enter the following settings:

Property	Variable	Value	Unit	Property group
Dynamic viscosity	mu	0.0434	Pa·s	Basic
Thermal conductivity	k_iso ; kii = k_iso, kij = 0	200	W/(m·K)	Basic
Density	rho	8500	kg/m³	Basic
Heat capacity at constant pressure	Ср	Cp_1	J/(kg·K)	Basic

LAMINAR FLOW (SPF)

Initial Values 1

- I In the Model Builder window, under Component I (compl)>Laminar Flow (spf) click Initial Values 1.
- 2 In the Settings window for Initial Values, locate the Initial Values section.
- **3** Specify the **u** vector as

0	r
v_cast	z

Inlet 1

- I In the Physics toolbar, click Boundaries and choose Inlet.
- 2 Select Boundary 15 only.
- 3 In the Settings window for Inlet, locate the Boundary Condition section.
- **4** From the list, choose **Pressure**.

Outlet I

- I In the Physics toolbar, click Boundaries and choose Outlet.
- 2 Select Boundary 2 only.
- 3 In the Settings window for Outlet, locate the Boundary Condition section.
- **4** From the list, choose **Velocity**.
- **5** Locate the **Velocity** section. Click the **Velocity** field button.
- **6** Specify the \mathbf{u}_0 vector as

0		r
v_c	ast	z

Wall 2

- I In the Physics toolbar, click Boundaries and choose Wall.
- 2 Select Boundaries 20–22 only.
- 3 In the Settings window for Wall, locate the Boundary Condition section.
- 4 From the Wall condition list, choose Slip.

Volume Force 1

- I In the Physics toolbar, click **Domains** and choose **Volume Force**.
- 2 In the Settings window for Volume Force, locate the Domain Selection section.
- 3 From the Selection list, choose All domains.
- **4** Locate the **Volume Force** section. Specify the \mathbf{F} vector as

Fr	r
Fz	z

DEFINITIONS

Ambient Properties I (ampr I)

- I In the Physics toolbar, click **Shared Properties** and choose **Ambient Properties**.
- 2 In the Settings window for Ambient Properties, locate the Ambient Conditions section.
- **3** In the $T_{\rm amb}$ text field, type 300[K].

This defines the ambient temperature for heat transfer between the outer surfaces and the surroundings.

HEAT TRANSFER IN FLUIDS (HT)

Fluid 1

In the Model Builder window, under Component I (compl)>Heat Transfer in Fluids (ht) click Fluid I.

Phase Change Material I

- I In the Physics toolbar, click Attributes and choose Phase Change Material.
- 2 In the Settings window for Phase Change Material, locate the Phase Change section.
- **3** In the $T_{\text{pc.}1\rightarrow 2}$ text field, type T_m.
- **4** In the $\Delta T_{1 \to 2}$ text field, type 2*dT.

The parameter dT is multiplied by 2 because it is only the half width of the phase change interval.

- **5** In the $L_{1\rightarrow 2}$ text field, type dH.
- 6 Locate the Phase I section. From the Material, phase I list, choose Solid Metal Alloy (mat I).
- 7 Locate the Phase 2 section. From the Material, phase 2 list, choose Liquid Metal Alloy (mat2).

Initial Values 1

- I In the Model Builder window, under Component I (compl)>Heat Transfer in Fluids (ht) click Initial Values I.
- 2 In the Settings window for Initial Values, locate the Initial Values section.
- **3** In the *T* text field, type T in.

Inflow I

- I In the Physics toolbar, click Boundaries and choose Inflow.
- 2 Select Boundary 15 only.
- 3 In the Settings window for Inflow, locate the Upstream Properties section.
- **4** In the T_{ustr} text field, type T_in.

Heat Flux I

- I In the Physics toolbar, click Boundaries and choose Heat Flux.
- 2 Select Boundary 23 only.
- 3 In the Settings window for Heat Flux, locate the Heat Flux section.
- 4 From the Flux type list, choose Convective heat flux.
- **5** In the *h* text field, type h_br.

6 From the $T_{\rm ext}$ list, choose Ambient temperature (amprl).

Heat Flux 2

- I In the Physics toolbar, click Boundaries and choose Heat Flux.
- 2 Select Boundary 22 only.
- 3 In the Settings window for Heat Flux, locate the Heat Flux section.
- 4 From the Flux type list, choose Convective heat flux.
- **5** In the h text field, type h mold.
- 6 From the T_{ext} list, choose Ambient temperature (amprl).

Heat Flux 3

- I In the Physics toolbar, click Boundaries and choose Heat Flux.
- 2 Select Boundaries 20 and 21 only.
- 3 In the Settings window for Heat Flux, locate the Heat Flux section.
- 4 From the Flux type list, choose Convective heat flux.
- **5** In the *h* text field, type h air.
- 6 From the T_{ext} list, choose Ambient temperature (amprI).

Outflow I

- I In the Physics toolbar, click Boundaries and choose Outflow.
- 2 Select Boundary 2 only.

Surface-to-Ambient Radiation I

- I In the Physics toolbar, click Boundaries and choose Surface-to-Ambient Radiation.
- 2 Select Boundaries 20 and 21 only.
- 3 In the Settings window for Surface-to-Ambient Radiation, locate the Surface-to-Ambient Radiation section.
- **4** From the ε list, choose **User defined**. In the associated text field, type eps_s.
- 5 From the $T_{\rm amb}$ list, choose Ambient temperature (amprl).

MESH I

- I In the Model Builder window, under Component I (compl) click Mesh I.
- 2 In the Settings window for Mesh, locate the Physics-Controlled Mesh section.
- **3** From the **Element size** list, choose **Finer**.

In the Mesh toolbar, click **Act Edit**.

Boundary Layers 1

- I In the Model Builder window, under Component I (compl)>Mesh I right-click Boundary Layers I and choose Delete.
- 2 Click Yes to confirm.

Deleting the boundary layers is necessary in order to use the adaptive mesh functionality.

Size 1

- I In the Model Builder window, under Component I (compl)>Mesh I click Size I.
- **2** Select Boundaries 16–21 only.
- 3 In the Settings window for Size, locate the Element Size section.
- 4 From the Predefined list, choose Fine.
- 5 In the Model Builder window, right-click Mesh I and choose Build All.

STUDY

Compute the solution using a three-step process. First, solve the problem using dT as a continuation parameter with the parametric solver on the default mesh, gradually decreasing the value of dT. Then, use the adaptive solver to adapt the mesh. Finally, use the parametric solver again to decrease dT further down to a value of 10 K.

- I In the Model Builder window, click Study I.
- 2 In the Settings window for Study, locate the Study Settings section.
- 3 Clear the Generate default plots check box.

The default plots are disabled for this study because they will be added from the last study.

Step 1: Stationary

- I In the Model Builder window, under Study I click Step I: Stationary.
- 2 In the Settings window for Stationary, click to expand the Study Extensions section.
- 3 Select the Auxiliary sweep check box.
- 4 Click + Add.
- **5** In the table, enter the following settings:

Parameter name	Parameter value list	Parameter unit
dT (Temperature transition zone half width)	300 100 50 30	К

Stationary 2

- I In the Study toolbar, click Study Steps and choose Stationary>Stationary.
- 2 In the Settings window for Stationary, click to expand the Adaptation and Error Estimates section.
- 3 From the Adaptation and error estimates list, choose Adaptation and error estimates.
- 4 Clear the Allow coarsening check box.
- 5 In the Study toolbar, click **Compute**.

LEVEL 2 ADAPTED MESH 2

Before proceeding with the final solution stage, inspect the adapted mesh. You find it under the automatically created Meshes branch in the model tree.

- I In the Model Builder window, expand the Component I (compl)>Meshes node, then click Level 2 Adapted Mesh 2.
- 2 In the Model Builder window, expand the Meshes node, then click Mesh 2.
- 3 Click the **Zoom Box** button in the **Graphics** toolbar and then use the mouse to zoom in on the transition zone where the mesh is the densest.

The mesh should look like that in Figure 6.

Add a second study for the second parametric study step.

ADD STUDY

- I In the Study toolbar, click Add Study to open the Add Study window.
- 2 Go to the Add Study window.
- 3 Find the Studies subsection. In the Select Study tree, select General Studies>Stationary.
- 4 Click Add Study in the window toolbar.
- 5 In the Study toolbar, click Add Study to close the Add Study window.

STUDY 2

In order to get faster convergence, you need to use the previous solution as the initial value for this study.

Step 1: Stationary

- I In the Model Builder window, under Study 2 click Step 1: Stationary.
- 2 In the Settings window for Stationary, click to expand the Values of Dependent Variables section.

- 3 Find the Initial values of variables solved for subsection. From the Settings list, choose User controlled.
- 4 From the Method list, choose Solution.
- 5 From the Study list, choose Study 1, Stationary 2.
- **6** Locate the **Study Extensions** section. Select the **Auxiliary sweep** check box.
- 7 Click + Add.
- **8** In the table, enter the following settings:

Parameter name	Parameter value list	Parameter unit
dT (Temperature transition zone half width)	25 20 16 13 10	К

Notice that Mesh 2, the adapted mesh, is the default selection in the mesh list. Keep this setting.

Again, a fully coupled solver is more robust for this model. Tweak the solver sequence accordingly with the instructions below.

Solution 7 (sol7)

- I In the Study toolbar, click Show Default Solver.
- 2 In the Model Builder window, expand the Solution 7 (sol7) node.
- 3 Right-click Study 2>Solver Configurations>Solution 7 (sol7)>Stationary Solver I and choose Fully Coupled.
- 4 In the Study toolbar, click **Compute**.

RESULTS

Velocity (spf)

To reproduce the plot in Figure 4, plot the velocity field as a combined surface and streamline plot.

Surface

- I In the Model Builder window, expand the Velocity (spf) node, then click Surface.
- 2 In the Settings window for Surface, locate the Expression section.
- **3** From the **Unit** list, choose **mm/s**.

Velocity (spf)

In the Model Builder window, click Velocity (spf).

Streamline 1

- I In the Velocity (spf) toolbar, click **Streamline**.
- 2 In the Settings window for Streamline, locate the Streamline Positioning section.
- 3 From the Positioning list, choose Magnitude controlled.
- 4 In the **Density** text field, type 12.
- 5 Locate the Coloring and Style section. Find the Point style subsection. From the Type list, choose Arrow.
- 6 In the Velocity (spf) toolbar, click Plot.

Pressure (sbf)

The second default plot shows the pressure profile in the 2D slice.

Velocity, 3D (spf)

The third default plot shows the velocity magnitude in 3D obtained by revolution of the 2D axisymmetric dataset.

Temperature, 3D (ht)

This default plot shows the temperature in 3D obtained by revolution of the 2D axisymmetric dataset.

Proceed to reproduce the lower plot in Figure 3, showing the fraction of liquid phase.

Fraction of Liquid Phase

- I In the Home toolbar, click Add Plot Group and choose 2D Plot Group.
- 2 In the Settings window for 2D Plot Group, type Fraction of Liquid Phase in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Study 2/Solution 7 (sol7).

Surface I

- I In the Fraction of Liquid Phase toolbar, click Surface.
- 2 In the Settings window for Surface, click Replace Expression in the upper-right corner of the Expression section. From the menu, choose Component I (compl)>Definitions> Variables>alpha - Fraction of liquid phase.
- 3 In the Fraction of Liquid Phase toolbar, click Plot. Notice, in particular, the narrow transition zone between the two phases.

To reproduce the upper plot in Figure 3, which visualizes the temperature and velocity fields, proceed as follows.

Temperature, Velocity Fields

- I In the Home toolbar, click **Add Plot Group** and choose **2D Plot Group**.
- 2 In the Settings window for 2D Plot Group, type Temperature, Velocity Fields in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Study 2/Solution 7 (sol7).

Surface I

- I In the Temperature, Velocity Fields toolbar, click
- 2 In the Settings window for Surface, click Replace Expression in the upper-right corner of the Expression section. From the menu, choose Component I (compl)> Heat Transfer in Fluids>Temperature>T - Temperature - K.
- 3 Locate the Coloring and Style section. From the Color table list, choose HeatCameraLight.
- 4 In the Temperature, Velocity Fields toolbar, click Plot.

Temberature, Velocity Fields

In the Model Builder window, click Temperature, Velocity Fields.

Streamline 1

- I In the Temperature, Velocity Fields toolbar, click Streamline.
- 2 In the Settings window for Streamline, locate the Streamline Positioning section.
- 3 From the Positioning list, choose Magnitude controlled.
- 4 In the **Density** text field, type 12.
- 5 Locate the Coloring and Style section. Find the Point style subsection. From the Type list, choose Arrow.
- 6 In the Temperature, Velocity Fields toolbar, click Plot.

Proceed to reproduce the heat flux plots shown in Figure 5.

Conductive Heat Flux

- I In the Home toolbar, click Add Plot Group and choose 2D Plot Group.
- 2 In the Settings window for 2D Plot Group, type Conductive Heat Flux in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Study 2/Solution 7 (sol7).

Surface I

- I In the Conductive Heat Flux toolbar, click Surface.
- 2 In the Settings window for Surface, click Replace Expression in the upper-right corner of the Expression section. From the menu, choose Component I (compl)>

Heat Transfer in Fluids>Domain fluxes>ht.dfluxMag - Conductive heat flux magnitude - W/ m².

3 In the Conductive Heat Flux toolbar, click Plot.

Conductive Heat Flux

In the Model Builder window, click Conductive Heat Flux.

Streamline I

- I In the Conductive Heat Flux toolbar, click **Streamline**.
- 2 In the Settings window for Streamline, locate the Streamline Positioning section.
- 3 From the Positioning list, choose Magnitude controlled.
- 4 In the Density text field, type 12.
- 5 Locate the Coloring and Style section. Find the Point style subsection. From the Type list, choose Arrow.
- 6 In the Conductive Heat Flux toolbar, click Plot.

The following steps reproduce the lower plot in the same figure, showing the conductive heat flux through the outer boundaries.

Conductive Heat Flux through Outer Boundaries

- I In the Home toolbar, click **Add Plot Group** and choose ID Plot Group.
- 2 In the Settings window for ID Plot Group, type Conductive Heat Flux through Outer Boundaries in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Study 2/Solution 7 (sol7).
- 4 From the Parameter selection (dT) list, choose Last.
- 5 Click to expand the **Title** section. From the **Title type** list, choose **Manual**.
- 6 In the Title text area, type Conductive heat flux through outer boundaries.
- 7 Locate the Plot Settings section. Select the x-axis label check box.
- 8 In the associated text field, type z-coordinate (m).
- **9** Select the **y-axis label** check box.
- 10 In the associated text field, type Normal conductive heat flux (W/m^2).

Line Graph 1

- I In the Conductive Heat Flux through Outer Boundaries toolbar, click the Line Graph.
- **2** Select Boundaries 20–23 only.

- 3 In the Settings window for Line Graph, click Replace Expression in the upper-right corner of the y-Axis Data section. From the menu, choose Component I (compl)> Heat Transfer in Fluids>Boundary fluxes>ht.ndflux - Normal conductive heat flux - W/m2.
- 4 Click Replace Expression in the upper-right corner of the x-Axis Data section. From the menu, choose Component I (compl)>Geometry>Coordinate>z - z-coordinate.
- 5 Click to expand the **Legends** section. Click to collapse the **Legends** section. Click to expand the Quality section. From the Recover list, choose Within domains.
- 6 Click to collapse the Quality section. In the Conductive Heat Flux through Outer Boundaries toolbar, click Plot.

Compare the result with the lower plot of Figure 5.

Finally, verify that the final mesh is sufficiently fine to resolve the temperaturedependence of the latent heat.

Cut Line 2D I

- I In the Results toolbar, click Cut Line 2D.
- 2 In the Settings window for Cut Line 2D, locate the Line Data section.
- 3 In row Point 1, set r to 0.045, and z to -0.42.
- 4 In row Point 2, set r to 0.085, and z to -0.43.

These values are chosen such that the two points are on opposite sides of and approximately perpendicular to the transition zone.

Alternatively, you can select the two end points and create the Cut Line 2D dataset with the help of the Fraction of Liquid Phase plot. Select the plot node, then click in the Graphics window after first selecting, in turn, First Point for Cut Line and Second Point for **Cut Line** in the main toolbar.

5 Locate the Data section. From the Dataset list, choose Study 2/Solution 7 (sol7).

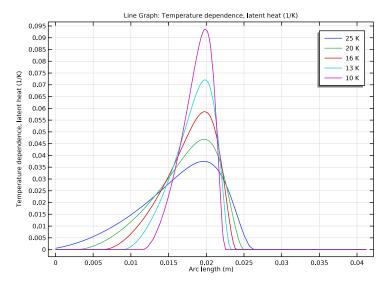
Temperature Dependence, Latent Heat

- I In the Results toolbar, click \to ID Plot Group.
- 2 In the Settings window for ID Plot Group, type Temperature Dependence, Latent Heat in the Label text field.
- 3 Locate the Data section. From the Dataset list, choose Cut Line 2D 1.

Line Graph 1

I In the Temperature Dependence, Latent Heat toolbar, click Line Graph.

- 2 In the Settings window for Line Graph, click Replace Expression in the upper-right corner of the y-Axis Data section. From the menu, choose Component I (compl)>Definitions> Variables>D - Temperature dependence, latent heat - I/K.
- 3 Click to expand the **Legends** section. Select the **Show legends** check box.
- 4 In the Temperature Dependence, Latent Heat toolbar, click **Plot**.



As you can see, the curves for the lower ΔT values, in particular at 10 K, are not entirely smooth. Thus, if you were to reduce ΔT further to model the casting of some pure metal, you would need to increase the mesh resolution.