# Failure of a Multilateral Well

Introduction

Multilateral wells — those with multiple legs that branch off from a single conduit — can produce oil efficiently because the legs can tap multiple productive zones and navigate around impermeable ones. Unfortunately, drilling engineers must often mechanically stabilize multilateral wells with a liner or casing, which can cost millions of dollars. Leaving the wellbore uncased reduces construction costs, but it runs a relatively high risk of catastrophic failure both during installation and after pumping begins.
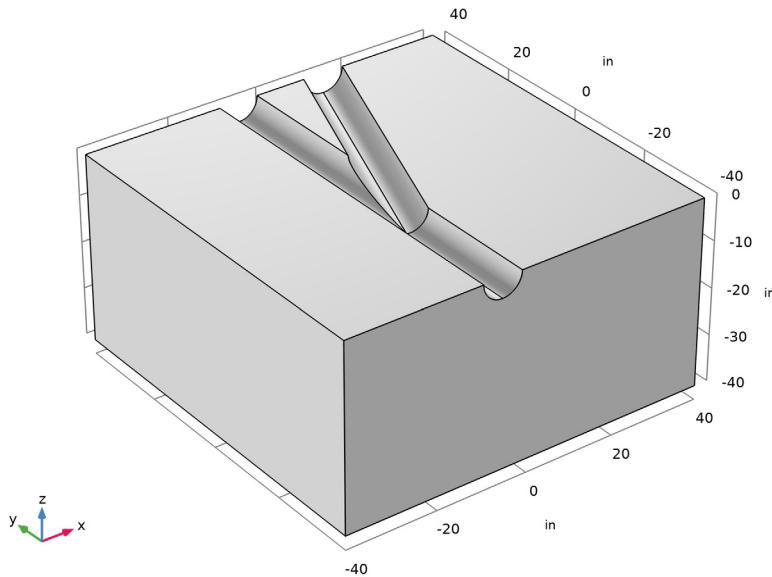
Figure 1: Geometry for an analysis of a horizontal open-hole multilateral well.

The poroelastic simulations estimate 3D compaction related to pumping by taking subsurface fluid flow with Darcy's law and coupling it to structural displacements with a stress-strain analysis. This example focuses on elastic displacements brought on by changing fluid pressures when pumping begins. Related analyses for elasto-plastic deformations are straightforward using material laws automated in the Structural Mechanics Module, Nonlinear Structural Materials Module, and Geomechanics Module.

Model Definition: Flow and Deformation Simulation

The modeled geometry (Figure 1) is the lower half of a branching junction, a segment from a larger well network. The junction lies roughly 25 feet from the start of the well. The entire well network extends much further, perhaps hundreds of feet. The well is 8.5 inches in diameter and sits in a cube 80 inches on each side. Pumps move fluid from the reservoir into the well. Fluid exits the geometry only through the well. The displacement at the reservoir edge is constrained. The walls of the well, however, deform freely. The goal is to solve for the change in fluid pressure, stress, strain, and displacement that the pumping causes rather than their absolute values.

FLUID FLOW

To describe fluid flow, you insert the Darcy velocity into an equation of continuity

$$\nabla \cdot \left[-\frac{\kappa}{\mu} \nabla p \right] = 0$$

where κ is the permeability, μ is the dynamic viscosity, and p equals the pressure of the oil in the pores.

For the flow boundaries, you already know the change in fluid pressure from the well to the reservoir edge. The planar surface adjacent to the well (between the upper and lower blocks) is a symmetry boundary. Because the well is the only exit for the fluid, there is no flow to or from connecting well segments. In summary,

$$p = p_r \qquad \partial\Omega \ \text{reservoir}$$

$$\mathbf{n} \cdot \left(-\frac{\kappa}{\mu} \nabla p \right) = 0 \qquad \partial\Omega \ \text{symmetry face}$$

$$\mathbf{n} \cdot \left(-\frac{\kappa}{\mu} \nabla p \right) = 0 \qquad \partial\Omega \ \text{connecting segments}$$

$$p = p_w \qquad \partial\Omega \ \text{well}$$

where $\mathbf{n}$ is the normal vector to the boundary.

SOLID DEFORMATION

The system of equations that describes the quasi-static deformation is

$$-\nabla \cdot \sigma = \mathbf{F}$$

where σ denotes the stress tensor, and **F** are external body forces. The stress tensor is augmented by the pressure load due to changes in pore pressure. In this model, the Biot-Willis coefficient is equal to one.

The stress-strain relationship for linear materials relates the stress tensor and the strain tensor ε through the elasticity matrix C, which for isotropic materials is a function of Young's modulus, E, and Poisson's ratio, ν.

In this geometrically linear example, the components of the strain tensor depend on the displacement vector **u**, which has directional components u, v, and w:

$$\varepsilon_x = \frac{\partial u}{\partial x} \qquad \varepsilon_{xy} = \frac{1}{2}\left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x}\right)$$

$$\varepsilon_y = \frac{\partial v}{\partial y} \qquad \varepsilon_{yz} = \frac{1}{2}\left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y}\right)$$

$$\varepsilon_z = \frac{\partial w}{\partial z} \qquad \varepsilon_{xz} = \frac{1}{2}\left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x}\right)$$

The tensors σ and ε are linearly related by Hooke's law σ = C:ε.

For the boundary conditions, the example constrains movement at all external boundaries. The well opening is free to deform. In summary:

$$
\begin{array}{lll}
u = v = w = 0 & \partial\Omega & \text{reservoir} \\
w = 0 & \partial\Omega & \text{symmetry face} \\
v = 0 & \partial\Omega & \text{connecting segments} \\
\text{free} & \partial\Omega & \text{well}
\end{array}
$$

MODEL DATA

This model uses the coefficients and parameters listed in Table 1.

TABLE 1: MODEL DATA.

VARIABLE	DESCRIPTION	VALUE
ρ_f	Fluid density	0.0361 lb/in^3
κ	Permeability	$1 \cdot 10^{-13}$ in^2
μ	Fluid dynamic viscosity	$1 \cdot 10^{-7}$ psi·s
E	Young's modulus	$0.43 \cdot 10^6$ psi
ν	Poisson's ratio	0.16
ρ_s	Solids density	0.0861 lb/in^3

VARIABLE	DESCRIPTION	VALUE
p_r	Pressure in reservoir	122.45 psi
p_w	Pressure in well	0 psi

Results: Flow and Deformation Simulation

The following figures show results from simulations for coupled fluid flow and reservoir deformation following a poroelastic approach for the horizontal multilateral well reported in Ref. 1.

The isosurfaces in Figure 2 indicate the fluid pressure throughout the well's lower half. The streamlines show the fluid paths and velocities. Fluid pressure drops from the reservoir toward the well opening. The velocity typically increases toward the well but remains close to zero near the branching legs of the junction.

Isosurface: Pressure (psi) Streamline: Darcy's velocity field (material and geometry frames)
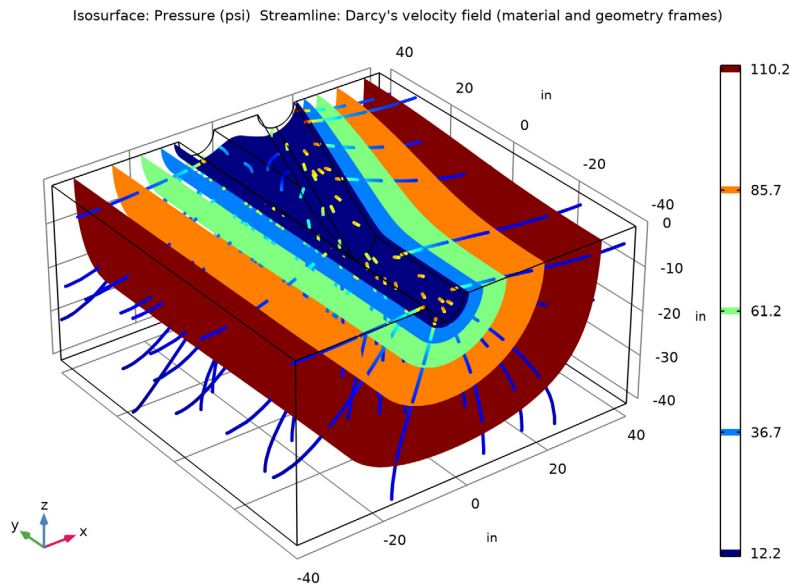
Figure 2: COMSOL Multiphysics poroelastic analysis of a multilateral well. Results are fluid pressure (the isosurfaces), pressure gradient (streamlines), and fluid velocities (streamline shading).

Results for elastic deformation appear in Figure 3. The surface shading denotes total displacement. The plot illustrates directional displacements by shifting the shading relative

to an outline of the original geometry. For a clear view, the displacements are exaggerated. The uncased surface yields slightly because the deformed shading fills in the hollows of the well. The largest displacements occur just above the split in the well.
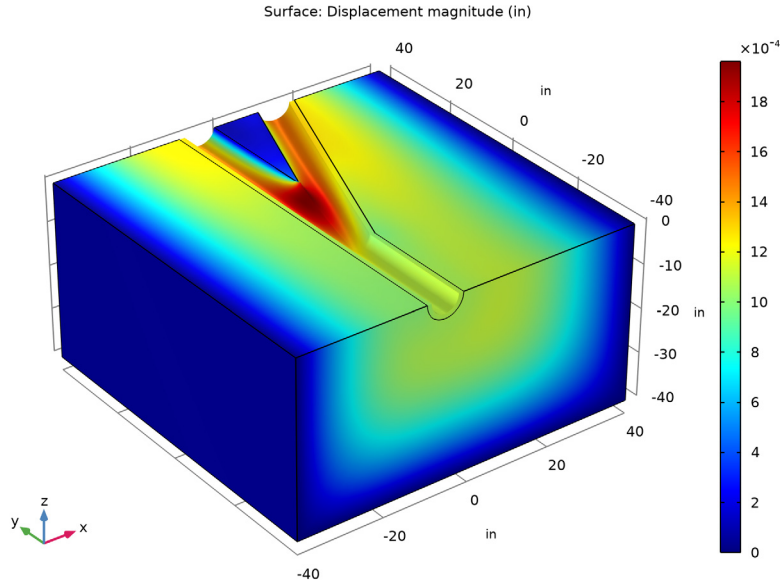
Figure 3: COMSOL Multiphysics estimates of displacement. Shading indicates the total displacement, and the geometry appears as lines. Even as the deformed shape shifts, those lines remain steady; the shaded image shows movement relative to the geometry outlines.

Failure Criterion

This model allows the evaluation of failures during postprocessing using results from the fluid-flow and solid-deformation simulations shown in the preceding figures. This discussion follows calculations that Ref. 1 uses to map calculations indicating where pumping could compact the reservoir enough (see Figure 3) that the well fails. Refer to Ref. 1 to estimate the critical rock strength required to successfully emplace the well, and also to learn more about calibration to data.

The 3D Coulomb failure criterion in Ref. 1 relates rock failure, the three principal stresses (σ_1, σ_2, and σ_3), and the fluid pressures as follows:

$$\text{fail} = (\sigma_3 + p) - Q(\sigma_1 + p) + N\left(1 + \frac{(\sigma_2 - \sigma_1)}{(\sigma_3 - \sigma_1)}\right)$$

$$Q = \frac{1 + \sin\phi}{1 - \sin\phi}, \qquad N = \frac{2\cos\phi}{1 - \sin\phi}\text{So}$$

(1)

Here **So** is the Coulomb cohesion and ϕ is the Coulomb friction angle. When properly calibrated, **fail** = 0 indicates the onset of rock failure; **fail** < 0 denotes catastrophic failure; and **fail** > 0 predicts stability. Because this model solves for the pressure change brought on by pumping as well as the stresses, strains, and displacements that the pressure change triggers, it calculates the expression just given using the change in pressure than its absolute value.

Results: Failure Criterion

The values for the **fail** function appear in Figure 4. When the **fail** values become increasingly negative, the potential for failure is higher. As expected, the **fail** function estimates show the greatest potential for failure just above the split in the well.
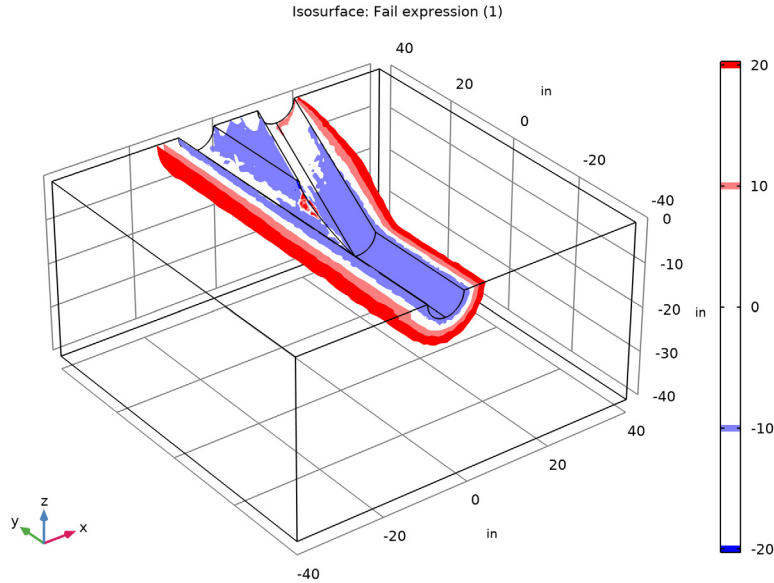

Figure 4: Values of the fail function calculated with results from a poroelastic model for the branching junction in an open-hole multilateral well. A negative value for the fail function denotes greater potential for failure.

Conclusions

This example couples fluid flow and solid deformation for a poroelastic analysis using easy-to-use physics interfaces from COMSOL Multiphysics. The analysis provides estimates of the pressure change brought on by pumping as well as the stresses, strains, and displacements that the pressure drop triggers. Combining the simulation results with a 3D Coulomb failure expression, maps vulnerability to mechanical failure from the pumping. The data and geometry for this model come from petroleum industry analyses by TerraTek (Ref. 1), which in turn use failure criteria to map the potential for failure during emplacement of the well in addition to the potential for failure when the well is pumped.

Reference

1. R. Suarez-Rivera, B.J. Begnaud, and W.J. Martin, "Numerical Analysis of Open-hole Multilateral Completions Minimizes the Risk of Costly Junction Failures," *Rio Oil & Gas Expo and Conference* (IBP096_04), 2004.

Application Library path: Subsurface_Flow_Module/
Flow_and_Solid_Deformation/multilateral_well

Modeling Instructions

From the **File** menu, choose **New**.

NEW

In the **New** window, click **Model Wizard**.

MODEL WIZARD

1 In the **Model Wizard** window, click **3D**.

2 In the **Select Physics** tree, select **Structural Mechanics>Poroelasticity>Poroelasticity, Solid**.

3 Click **Add**.

4 Click **Study**.

5 In the **Select Study** tree, select **General Studies>Stationary**.

6 Click **Done**.

GEOMETRY 1

1 In the **Model Builder** window, under **Component 1 (comp1)** click **Geometry 1**.

2 In the **Settings** window for **Geometry**, locate the **Units** section.

3 From the **Length unit** list, choose **in**.

Import 1 (imp1)

1 In the **Home** toolbar, click ⭤ **Import**.

2 In the **Settings** window for **Import**, locate the **Import** section.

3 Click **Browse**.

4 Browse to the model's Application Libraries folder and double-click the file
`multilateral_well.mphbin`.

5 Click **Import**.

GLOBAL DEFINITIONS

Parameters 1

1 In the **Model Builder** window, under **Global Definitions** click **Parameters 1**.

2 In the **Settings** window for **Parameters**, locate the **Parameters** section.

3 In the table, enter the following settings:

Name	Expression	Value	Description
p_r	122.45[psi]	8.4426E5 Pa	Pressure in reservoir
p_w	0[psi]	0 Pa	Pressure in well
So	850[psi]	5.8605E6 Pa	Coulomb cohesion
phi	31[deg]	0.54105 rad	Friction angle
C1	14.7	14.7	Calibration constant 1
C2	40	40	Calibration constant 2
suppX	0	0	Well support, x-component
suppY	0	0	Well support, y-component
suppZ	0	0	Well support, z-component

DEFINITIONS

Variables 1

1 In the **Home** toolbar, click $a=$ **Variables** and choose **Local Variables**.

2 In the **Settings** window for **Variables**, locate the **Variables** section.

3 In the table, enter the following settings:

Name	Expression	Unit	Description
N	2*So*cos(phi)/(1-sin(phi))	Pa	Fail parameter 1
Q	(1+sin(phi))/(1-sin(phi))		Fail parameter 2
fail	(((solid.sp3+C1*(p_r-p))-Q*(solid.sp1+C1*(p_r-p))+N*(1+(solid.sp2-solid.sp1)/(solid.sp3-solid.sp1)))/C2)[1/psi]		Fail expression

Here, `solid.sp1`, `solid.sp2`, and `solid.sp3` are the principal stresses. Note that the expression fail defined in Equation 1 has the dimension of stress. By appending the operator `[1/psi]` to the dimensionful expression enclosed within parentheses you extract its value in psi, which is what Ref. 1 uses. This way, you can analyze the risk for rock failure using the same criterion independently of your choice of base unit system.

MATERIALS

Create two materials: one for the porous matrix, and one for the fluid.

Porous Matrix

1 In the **Model Builder** window, under **Component 1 (comp1)** right-click **Materials** and choose **Blank Material**.

2 In the **Settings** window for **Material**, type Porous Matrix in the **Label** text field.

Fluid

1 Right-click **Materials** and choose **Blank Material**.

2 In the **Settings** window for **Material**, type Fluid in the **Label** text field.

The fluid material has no selection. Select it manually in the **Poroelastic Storage** model.

DARCY'S LAW (DL)

Poroelastic Storage 1

1 In the **Model Builder** window, under **Component 1 (comp1)>Darcy's Law (dl)** click **Poroelastic Storage 1**.

2 In the **Settings** window for **Poroelastic Storage**, locate the **Fluid Properties** section.

3 From the **Fluid material** list, choose **Fluid (mat2)**.

MATERIALS

Porous Matrix (mat1)

1 In the **Model Builder** window, under **Component 1 (comp1)>Materials** click
  Porous Matrix (mat1).

2 In the **Settings** window for **Material**, locate the **Material Contents** section.

3 In the table, enter the following settings:

Property	Variable	Value	Unit	Property group
Young's modulus	E	`4.3e5[psi]`	Pa	Basic
Poisson's ratio	nu	`0.16`	1	Basic
Density	rho	`0.0861[lb/in^3]`	kg/m³	Basic
Porosity	epsilon	`0.3`	1	Basic
Permeability	kappa_iso ; kappaii = kappa_iso, kappaij = 0	`1e-13[in^2]`	m²	Basic
Biot-Willis coefficient	alphaB	`1`	1	Poroelastic material

Fluid (mat2)

1 In the **Model Builder** window, click **Fluid (mat2)**.

2 In the **Settings** window for **Material**, locate the **Material Contents** section.

3 In the table, enter the following settings:

Property	Variable	Value	Unit	Property group
Compressibility of fluid	chif	`4e-10`	1/Pa	Basic
Density	rho	`0.0361[lb/in^3]`	kg/m³	Basic
Dynamic viscosity	mu	`1e-7[psi*s]`	Pa·s	Basic

SOLID MECHANICS (SOLID)

In the **Model Builder** window, under **Component 1 (comp1)** click **Solid Mechanics (solid)**.

Fixed Constraint 1

1 In the **Physics** toolbar, click ▭ **Boundaries** and choose **Fixed Constraint**.

2 Select Boundaries 1, 3, and 13 only.

Prescribed Displacement 1

1 In the **Physics** toolbar, click ▭ **Boundaries** and choose **Prescribed Displacement**.

2 Select Boundaries 2 and 5 only.

3 In the **Settings** window for **Prescribed Displacement**, locate the **Prescribed Displacement** section.

4 Select the **Prescribed in y direction** check box.

Prescribed Displacement 2

1 In the **Physics** toolbar, click ▭ **Boundaries** and choose **Prescribed Displacement**.

2 Select Boundaries 4, 11, and 12 only.

3 In the **Settings** window for **Prescribed Displacement**, locate the **Prescribed Displacement** section.

4 Select the **Prescribed in z direction** check box.

Boundary Load 1

1 In the **Physics** toolbar, click ▭ **Boundaries** and choose **Boundary Load**.

2 Select Boundaries 6–10 only.

3 In the **Settings** window for **Boundary Load**, locate the **Force** section.

4 Specify the $\mathbf{F}_A$ vector as

-suppX	x
-suppY	y
-suppZ	z

DARCY'S LAW (DL)

Initial Values 1

1 In the **Model Builder** window, under **Component 1 (comp1)>Darcy's Law (dl)** click **Initial Values 1**.

2 In the **Settings** window for **Initial Values**, locate the **Initial Values** section.

3 In the p text field, type p_r.

Pressure 1

1 In the **Physics** toolbar, click ▭ **Boundaries** and choose **Pressure**.

2 Select Boundaries 1, 3, and 13 only.

3 In the **Settings** window for **Pressure**, locate the **Pressure** section.

4 In the p_0 text field, type p_r.

Pressure 2

1 In the **Physics** toolbar, click 🔳 **Boundaries** and choose **Pressure**.

2 Select Boundaries 6–10 only.

3 In the **Settings** window for **Pressure**, locate the **Pressure** section.

4 In the p_0 text field, type p_w.

STUDY 1

1 In the **Model Builder** window, click **Study 1**.

2 In the **Settings** window for **Study**, locate the **Study Settings** section.

3 Clear the **Generate default plots** check box.

4 In the **Home** toolbar, click ▬ **Compute**.

RESULTS

Create a plot which shows the displacement as in Figure 3.

Displacement

1 In the **Home** toolbar, click 🔳 **Add Plot Group** and choose **3D Plot Group**.

2 In the **Settings** window for **3D Plot Group**, type Displacement in the **Label** text field.

Surface 1

Right-click **Displacement** and choose **Surface**.

Deformation 1

1 In the **Model Builder** window, right-click **Surface 1** and choose **Deformation**.

2 In the **Settings** window for **Deformation**, locate the **Scale** section.

3 Select the **Scale factor** check box.

4 In the associated text field, type 1000.

5 In the **Displacement** toolbar, click 🔳 **Plot**.

Next, create a plot that visualizes the pressure and velocity fields like in Figure 2.

Fluid Pressure and Velocities

1 In the **Home** toolbar, click 🔳 **Add Plot Group** and choose **3D Plot Group**.

2 In the **Settings** window for **3D Plot Group**, type Fluid Pressure and Velocities in the **Label** text field.

Isosurface 1

1 Right-click **Fluid Pressure and Velocities** and choose **Isosurface**.

2 In the **Settings** window for **Isosurface**, locate the **Expression** section.

3 In the **Expression** text field, type p.

4 From the **Unit** list, choose **psi**.

Streamline 1

1 In the **Model Builder** window, right-click **Fluid Pressure and Velocities** and choose **Streamline**.

2 In the **Settings** window for **Streamline**, click **Replace Expression** in the upper-right corner of the **Expression** section. From the menu, choose **Component 1 (comp1)>Darcy's Law> Velocity and pressure>dl.u,...,dl.w - Darcy's velocity field (material and geometry frames)**.

3 Locate the **Streamline Positioning** section. From the **Positioning** list, choose **Starting-point controlled**.

4 In the **Points** text field, type 60.

5 Locate the **Coloring and Style** section. Find the **Line style** subsection. From the **Type** list, choose **Tube**.

6 In the **Tube radius expression** text field, type 0.4.

Color Expression 1

1 Right-click **Streamline 1** and choose **Color Expression**.

2 In the **Settings** window for **Color Expression**, locate the **Expression** section.

3 In the **Expression** text field, type dl.U.

4 Locate the **Coloring and Style** section. Clear the **Color legend** check box.

5 Click the ◀ **Scene Light** button in the **Graphics** toolbar.

6 In the **Fluid Pressure and Velocities** toolbar, click ▣ **Plot**.

Finally, investigate the risk for failure by plotting the fail expression, shown in Figure 4.

Fail Function

1 In the **Home** toolbar, click ▦ **Add Plot Group** and choose **3D Plot Group**.

2 In the **Settings** window for **3D Plot Group**, type Fail Function in the **Label** text field.

Isosurface 1

1 Right-click **Fail Function** and choose **Isosurface**.

2 In the **Settings** window for **Isosurface**, locate the **Expression** section.

3 In the **Expression** text field, type fail.

4 In the **Fail Function** toolbar, click ▣ **Plot**.

5 Locate the **Levels** section. From the **Entry method** list, choose **Levels**.

6 Click ⌇ **Range**.

7 In the **Range** dialog box, type -20 in the **Start** text field.

8 In the **Stop** text field, type 20.

9 In the **Step** text field, type 10.

10 Click **Replace**.

11 In the **Settings** window for **Isosurface**, locate the **Coloring and Style** section.

12 From the **Color table** list, choose **WaveLight**.

13 In the **Fail Function** toolbar, click ▣ **Plot**.