

Thermo-Mechanical Analysis of a Surface-Mounted Resistor

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Introduction

The drive for miniaturizing electronic devices has resulted in today's extensive use of surface-mount electronic components. An important aspect in electronics design and the choice of materials is a product's durability and lifetime. For surface-mount resistors and other components producing heat it is a well-known problem that temperature cycling can lead to cracks propagating through the solder joints, resulting in premature failure (Ref. 1). For electronics in general there is a strong interest in changing the soldering material from lead- or tin-based solder alloys to other mixtures.

The following multiphysics example models the heat transport and structural stresses and deformations resulting from the temperature distribution using the Heat Transfer in Solids and Solid Mechanics interfaces.

Note: This application requires either the Structural Mechanics Module or the MEMS Module.

Model Definition

Figure 1 shows a photograph of a surface-mount resistor together with a diagram of it on a printed circuit board (PCB).



Figure 1: A photo and diagram of a typical surface-mounted resistor soldered to a PCB.

Table 1 shows the dimensions of the resistor and other key components in the model including the PCB.

COMPONENT	LENGTH	WIDTH	HEIGHT
Resistor (Alumina)	6 mm	3 mm	0.5 mm
PCB (FR4)	l6 mm	8 mm	1.6 mm
Cu pad	2 mm	3 mm	35 µm
Termination (Silver)	0.5 mm	3 mm	25 μm
Stand-off (gap to PCB)	-	-	105 μm

TABLE I: COMPONENT DIMENSIONS

The simulation makes use of the symmetry so that it needs to include only half of the component (Figure 2). The modeling of the PCB is terminated a distance away from the resistor, in order to reduce effects of the boundary conditions.



Figure 2: The simulation models only one half of the resistor.

In operation, the resistor dissipates 0.2 W of power as heat. Conduction to the PCB and convection to the surrounding air provide cooling. In this model, the heat transfer occurs through conduction in the subdomains. The model simplifies the surface cooling and describes it using a heat transfer coefficient, h, in this case set to $10 \text{ W/(m}^2 \cdot \text{K})$; the surrounding air temperature, T_{inf} , is at 300 K. The resulting heat transfer equation and boundary condition (included in the model using the Heat Transfer interface) are

$$\nabla \cdot (-k\nabla T) = Q$$
$$-\mathbf{n} \cdot (-k\nabla T) = h(T_{inf} - T)$$

where *k* is the thermal conductivity, and *Q* is the heating power per unit volume of the resistor (equal to 22.2 MW/m³ corresponding to 0.2 W in total).

The model handles thermal expansion using a static structural analysis using the Structural Mechanics interface (a description of the corresponding equations is available in the *Structural Mechanics Module User's Guide*). The thermal and mechanical material

properties in this model are taken from the material library The data for the solid materials are temperature independent, and the reference values are shown in the table below.

MATERIAL	E (GPa)	ν	lpha (ppm)	k (W/(m·K))	ρ (kg/m ³)	C_p (J/(kg·K))
Silver	83	0.37	18.9	420	10500	230
Alumina	300	0.222	8.0	27	3900	900
Cu	110	0.35	17	400	8700	385
Fr4	22	0.28	18	0.3	1900	1369
60Sn-40Pb	10	0.4	21	50	9000	150

TABLE	2 .	MATERIAL	PROPERTIES
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Air has temperature-dependent and pressure-dependent properties in the built-in material library. Because the temperature is a variable of the problem, it is automatically used. The pressure is by default set to 1 atm.

The stresses are zero at room temperature, **293** K. The boundary condition for the Solid Mechanics interface is that the cuts in the PCB do not rotate and have no net force normal to the cut.

Results and Discussion

The isosurfaces in Figure 3 show the temperature distribution at steady state. The highest temperature occurs in the center of the resistor. The circuit board also heats up significantly.



Figure 3: Temperature distribution in the resistor and the circuit board at steady state.

Thermal stresses appear as a result of the temperature increase; they arise from the materials' different expansion coefficients and from the bending of the PCB. Figure 4 plots the effective stress (von Mises) together with the resulting deformation of the assembly.



Figure 4: The thermally induced distribution of von Mises effective stress together with the deformation (magnified).

The highest stresses seem to occur in the termination material. It is interesting to compare these effective stresses to the yield stress and thereby investigate whether or not the material is irreversibly deformed. In that case the solder is the weak point. Figure 5 the stress in the solder alone.

Volume: von Mises stress (MPa)



Figure 5: Close-up of the von Mises effective stresses in the solder joints.

The yield stress for solder is approximately 220 MPa. The highest effective stress appears to be about 60 percent of this value. The structure does not get permanently deformed directly when heated. However, it is possible that the solder displays creep strains over time because of the combination of fairly high stress levels and elevated temperatures.

Notes About the COMSOL Implementation

In this example, the Thermal Stress interface automatically adds and couples the Solid Mechanics interface and the Heat Transfer interface. This is done by the two predefined multiphysics features Thermal Expansion and Temperature Coupling.

Build the geometry as an assembly of the bottom plate and the resistor to make it possible to mesh the parts independently. Use continuity conditions for the temperature and the displacements to connect the top and bottom parts of the geometry.

It is assumed that the temperature gradient in the normal direction on the cuts in the PCB is zero. The mechanical boundary conditions on the cuts must not impose a general state of compressive stress due to thermal expansion. At the same time, the restraint from the part of the PCB that is not modeled means that there is no rotation of the cross section.

To obtain this effect, the entire cut must have the same (but unknown) displacement in the direction normal to the cut.

You can achieve this by using the roller constraint at the left cut of the plate that prevents the boundary to move in the direction normal to the cut. For remaining two cuts, introduce two new degrees of freedom (named uface and vface) in the model and prescribe the displacements of the cut faces to them.

You solve the problem sequentially using two stationary study steps. The heat transfer problem is nonlinear because the air has temperature-dependent properties. The structural problem, on the other hand, is linear. For the structural analysis, use a memory-efficient iterative solver to make it possible to solve the problem also on computers with limited memory.

References

1. H. Lu, C. Bailey, M. Dusek, C. Hunt, and J. Nottay, "Modeling the Fatigue Life of Solder Joints of Surface Mount Resistors," EMAP, 2000.

2. J.M. Coulson and J.F. Richardson, *Chemical Engineering*, vol. 1, Pergamon Press, appendix, 1990.

Application Library path: Heat_Transfer_Module/Thermal_Stress/ surface_resistor

Modeling Instructions

From the File menu, choose New.

NEW

In the New window, click Model Wizard.

MODEL WIZARD

- I In the Model Wizard window, click 3D.
- 2 In the Select Physics tree, select Structural Mechanics>Thermal Stress.
- 3 Click Add.
- 4 Click Study.

5 In the Select Study tree, select Preset Studies for Selected Physics Interfaces>Stationary.

6 Click Done.

GLOBAL DEFINITIONS

Parameters

- I On the Home toolbar, click Parameters.
- 2 In the Settings window for Parameters, locate the Parameters section.
- **3** In the table, enter the following settings:

Name	Expression	Value	Description
T_air	300[K]	300 K	Air temperature
h_air	10[W/(m^2*K)]	10 W/(m²·K)	Heat transfer coefficient
Psource	0.2[W]/2	0.1 W	Heat dissipated by the resistor on the half geometry
p0	1[atm]	1.013E5 Pa	Air pressure
Т0	80[degC]	353.2 K	Initial temperature guess

GEOMETRY I

- I In the Model Builder window, under Component I (compl) click Geometry I.
- 2 In the Settings window for Geometry, locate the Units section.
- 3 From the Length unit list, choose mm.

Create the geometry. To simplify this step, insert a prepared 2D geometry sequence. On the Geometry toolbar, point to Import/Export and choose Insert Sequence. Browse to

the application's Application Library folder and double-click the file surface_resistor.mph.



The 2D geometry should now look as in the figure below.

Extrude I (extI)

- I On the Geometry toolbar, click Extrude.
- 2 Select the object wpl only.
- 3 In the Settings window for Extrude, locate the Distances section.
- **4** In the table, enter the following settings:

Distances (mm)

1.5

5 Click **Build All Objects**.

Block I (blkI)

- I On the Geometry toolbar, click Block.
- 2 In the Settings window for Block, locate the Size and Shape section.
- 3 In the Width text field, type 4.
- 4 In the **Depth** text field, type 16.

- 5 In the **Height** text field, type 1.6.
- 6 Locate the Position section. In the y text field, type -4.
- 7 In the z text field, type -1.6.
- 8 Click Build All Objects.
- 9 Click the Zoom Extents button on the Graphics toolbar.

Now, create an imprint of the resistor's bottom boundary on the printed circuit board to make a pair with matching parts.

Form Union (fin)

- I In the Model Builder window, under Component I (compl)>Geometry I click Form Union (fin).
- 2 In the Settings window for Form Union/Assembly, locate the Form Union/Assembly section.
- 3 From the Action list, choose Form an assembly.
- 4 Select the **Create imprints** check box.
- 5 On the Geometry toolbar, click Build All.

The completed geometry is shown in Figure 2.

ADD MATERIAL

- I On the Home toolbar, click Add Material to open the Add Material window.
- 2 Go to the Add Material window.
- 3 In the tree, select Built-In>FR4 (Circuit Board).
- 4 Click Add to Component in the window toolbar.

MATERIALS

- FR4 (Circuit Board) (mat1)
- I In the Model Builder window, under Component I (compl)>Materials click FR4 (Circuit Board) (matl).
- 2 In the Settings window for Material, locate the Geometric Entity Selection section.
- **3** From the **Selection** list, choose **Manual**.
- 4 Click Clear Selection.
- **5** Select Domain 1 only.

ADD MATERIAL

I Go to the Add Material window.

- 2 In the tree, select Built-In>Alumina.
- 3 Click Add to Component in the window toolbar.

MATERIALS

Alumina (mat2)

- I In the Model Builder window, under Component I (compl)>Materials click Alumina (mat2).
- 2 Select Domain 5 only.

ADD MATERIAL

- I Go to the Add Material window.
- 2 In the tree, select Built-In>Copper.
- 3 Click Add to Component in the window toolbar.

MATERIALS

Copper (mat3)

- I In the Model Builder window, under Component I (compl)>Materials click Copper (mat3).
- **2** Select Domains 2 and 7 only.

ADD MATERIAL

- I Go to the Add Material window.
- 2 In the tree, select Material Library>Elements>Silver>Silver [solid].
- 3 Click Add to Component in the window toolbar.

MATERIALS

Silver [solid] (mat4)

- I In the Model Builder window, under Component I (compl)>Materials click Silver [solid] (mat4).
- **2** Select Domains 4 and 9 only.

ADD MATERIAL

- I Go to the Add Material window.
- 2 In the tree, select Built-In>Solder, 60Sn-40Pb.
- 3 Click Add to Component in the window toolbar.

MATERIALS

Solder, 60Sn-40Pb (mat5)

- In the Model Builder window, under Component I (compl)>Materials click Solder, 60Sn-40Pb (mat5).
- 2 Select Domains 3 and 8 only.

ADD MATERIAL

- I Go to the Add Material window.
- 2 In the tree, select Built-In>Air.
- 3 Click Add to Component in the window toolbar.

MATERIALS

Air (mat6)

- I In the Model Builder window, under Component I (compl)>Materials click Air (mat6).
- 2 Select Domain 6 only.
- 3 On the Home toolbar, click Add Material to close the Add Material window.

SOLID MECHANICS (SOLID)

- I In the Model Builder window, under Component I (compl) click Solid Mechanics (solid).
- 2 Select Domains 1–5 and 7–9 only.

Symmetry I

- I Right-click Component I (compl)>Solid Mechanics (solid) and choose More Constraints> Symmetry.
- **2** Select Boundaries 1, 10, 13, 16, 20, 33, 37, and 40 only.

Continuity I

- I In the Model Builder window, right-click Solid Mechanics (solid) and choose Pairs> Continuity.
- 2 In the Settings window for Continuity, locate the Pair Selection section.
- 3 In the Pairs list, select Identity Boundary Pair I (apl).

Roller 1

I Right-click Solid Mechanics (solid) and choose Roller.

2 Select Boundary 8 only.

Create the special boundary conditions on the cuts in the PCB by introducing new degrees of freedom, uface and vface, for the normal displacements.

3 In the **Model Builder** window's toolbar, click the **Show** button and select **Advanced Physics Options** in the menu.

Global Equations 1

- I Right-click Solid Mechanics (solid) and choose Global>Global Equations.
- 2 In the Settings window for Global Equations, locate the Global Equations section.
- **3** In the table, enter the following settings:

Name	f(u,ut,utt,t) (l)	Initial value (u_0) (I)	Initial value (u_t0) (1/s)	Description
uface		0	0	
vface		0	0	

4 Locate the Units section. Find the Dependent variable quantity subsection. From the list, choose Displacement field (m).

Prescribed Displacement I

- I Right-click Solid Mechanics (solid) and choose Points>Prescribed Displacement.
- 2 Select Point 1 only.
- **3** In the **Settings** window for **Prescribed Displacement**, locate the **Prescribed Displacement** section.
- **4** Select the **Prescribed in z direction** check box.

Prescribed Displacement 2

- I Right-click Solid Mechanics (solid) and choose Prescribed Displacement.
- 2 Select Boundary 2 only.
- **3** In the **Settings** window for **Prescribed Displacement**, locate the **Prescribed Displacement** section.
- 4 Select the Prescribed in y direction check box.
- **5** In the u_{0y} text field, type vface.

Prescribed Displacement 3

- I Right-click Solid Mechanics (solid) and choose Prescribed Displacement.
- 2 Select Boundary 9 only.

- **3** In the **Settings** window for **Prescribed Displacement**, locate the **Prescribed Displacement** section.
- 4 Select the Prescribed in x direction check box.
- **5** In the u_{0x} text field, type uface.

HEAT TRANSFER IN SOLIDS (HT)

Fluid I

- I In the Model Builder window, under Component I (compl) right-click Heat Transfer in Solids (ht) and choose Fluid.
- **2** Select Domain 6 only.

Heat Source 1

- I In the Model Builder window, right-click Heat Transfer in Solids (ht) and choose Heat Source.
- 2 Select Domain 5 only.
- 3 In the Settings window for Heat Source, locate the Heat Source section.
- 4 Click the **Heat rate** button.
- **5** In the P_0 text field, type Psource.

Heat Flux 1

- I Right-click Heat Transfer in Solids (ht) and choose Heat Flux.
- 2 Select Boundaries 3, 4, 11, 14, 19, 29, 30, 44, 46, and 49–58 only.
- 3 In the Settings window for Heat Flux, locate the Heat Flux section.
- 4 Click the **Convective heat flux** button.
- **5** In the *h* text field, type h_air.
- 6 In the T_{ext} text field, type T_air.

Next, add the continuity condition on the identity pair to couple the domains together.

Continuity I

- I Right-click Heat Transfer in Solids (ht) and choose Pairs>Continuity.
- 2 In the Settings window for Continuity, locate the Pair Selection section.
- 3 In the Pairs list, select Identity Boundary Pair I (apl).

Because the material properties are temperature dependent, the solution converges better if you supply an initial guess of the temperature. Initial Values 1

- I In the Model Builder window, under Component I (comp1)>Heat Transfer in Solids (ht) click Initial Values I.
- 2 In the Settings window for Initial Values, type T0 in the T text field.

MESH I

Free Triangular 1

- I In the Model Builder window, under Component I (compl) right-click Mesh I and choose More Operations>Free Triangular.
- **2** Select Boundaries 10, 13, 16, 20, 24, 33, 37, and 40 only.

Size 1

- I Right-click Component I (comp1)>Mesh 1>Free Triangular I and choose Size.
- 2 In the Settings window for Size, locate the Element Size section.
- 3 From the Predefined list, choose Fine.
- **4** Click the **Custom** button.
- 5 Locate the Element Size Parameters section. Select the Minimum element size check box.
- 6 In the associated text field, type 0.1.
- 7 Click Build Selected.

Swept I

- I In the Model Builder window, right-click Mesh I and choose Swept.
- 2 In the Settings window for Swept, locate the Domain Selection section.
- 3 From the Geometric entity level list, choose Domain.
- **4** Select Domains 2–9 only.

Distribution I

- I Right-click Component I (comp1)>Mesh 1>Swept I and choose Distribution.
- 2 In the Settings window for Distribution, locate the Distribution section.
- 3 In the Number of elements text field, type 10.
- 4 Click Build All.

Size 1

- I In the Model Builder window, right-click Mesh I and choose Free Tetrahedral.
- 2 Right-click Free Tetrahedral I and choose Size.
- 3 In the Settings window for Size, locate the Geometric Entity Selection section.

- 4 From the Geometric entity level list, choose Boundary.
- **5** Select Boundaries 5–7 only.
- 6 Locate the Element Size section. From the Predefined list, choose Extra fine.
- 7 Click Build All.



STUDY I

Because the heat transfer problem is independent of the displacements, use the first stationary study step to find the temperature distribution and the second stationary step to solve for the displacements.

Step 1: Stationary

- I In the Model Builder window, expand the Study I node, then click Step I: Stationary.
- 2 In the Settings window for Stationary, locate the Physics and Variables Selection section.
- 3 In the table, clear the Solve for check box for the Solid Mechanics interface.

Step 2: Stationary 2

- I On the Study toolbar, click Study Steps and choose Stationary>Stationary.
- 2 In the Settings window for Stationary, locate the Physics and Variables Selection section.
- 3 In the table, clear the Solve for check box for the Heat Transfer in Solids interface.
- 4 Click to expand the Values of dependent variables section. Locate the Values of Dependent Variables section. Find the Values of variables not solved for subsection. From the Settings list, choose User controlled.

- 5 From the Method list, choose Solution.
- 6 From the Study list, choose Study I, Stationary.

Solution 1 (soll)

- I On the Study toolbar, click Show Default Solver.
- 2 In the Model Builder window, expand the Solution I (soll) node.
- 3 In the Model Builder window, expand the Study I>Solver Configurations> Solution I (soll)>Stationary Solver I node.
- 4 Right-click **Direct** and choose **Enable**.

Set up an iterative solver that can significantly save on the memory needed for the computations.

- 5 In the Model Builder window, under Study I>Solver Configurations>Solution I (sol1) click Stationary Solver 2.
- 6 In the Settings window for Stationary Solver, locate the General section.
- 7 From the Linearity list, choose Linear.
- 8 In the Model Builder window, expand the Study I>Solver Configurations> Solution I (soll)>Stationary Solver 2 node.
- 9 Right-click Suggested Iterative Solver (solid) and choose Enable.
- **IO** In the **Settings** window for **Iterative**, click to expand the **Error** section.
- II In the Factor in error estimate text field, type 2000.
- **12** On the **Study** toolbar, click **Compute**.

RESULTS

Stress (solid)

The first plot shows the effective stress together with the resulting deformation. Modify it to reproduce Figure 4.

I In the Model Builder window, expand the Stress (solid) node.

Deformation

- I In the Model Builder window, expand the Results>Stress (solid)>Surface I node, then click Deformation.
- 2 In the Settings window for Deformation, locate the Expression section.
- **3** In the **Y** component text field, type v-vface.
- 4 On the Stress (solid) toolbar, click Plot.

Stress (solid)

Hold down the left mouse button and drag in the Graphics window to rotate the geometry so that you see the opposite side of the resistor, which is where the largest stresses occur. Similarly, use the right mouse button to translate the geometry and the middle button to zoom.

Now, study the stresses in the solder.

Selection

- I On the Results toolbar, click More Data Sets and choose Solution.
- 2 On the **Results** toolbar, click **Selection**.
- 3 In the Settings window for Selection, locate the Geometric Entity Selection section.
- 4 From the Geometric entity level list, choose Domain.
- **5** Select Domain 3 only.

3D Plot Group 4

- I On the **Results** toolbar, click **3D** Plot Group.
- 2 In the Settings window for 3D Plot Group, type Stress in Solder Joint in the Label text field.
- 3 Locate the Data section. From the Data set list, choose Study I/Solution I (3) (soll).
- 4 Locate the Plot Settings section. Clear the Plot data set edges check box.

Volume 1

- I Right-click Stress in Solder Joint and choose Volume.
- 2 In the Settings window for Volume, click Replace Expression in the upper-right corner of the Expression section. From the menu, choose Component I>Solid Mechanics>Stress> solid.mises - von Mises stress.
- 3 Locate the Expression section. From the Unit list, choose MPa.
- 4 On the Stress in Solder Joint toolbar, click Plot.
- 5 Click the Go to YZ View button on the Graphics toolbar.

Compare the resulting plot with that in Figure 5.

Temperature (ht)

The second default plot group shows the temperature on the modeled geometry's surface.

I In the Model Builder window, under Results click Temperature (ht).





lsothermal Contours (ht) The third default plot shows the isosurfaces (Figure 3).